
Comparison of MOST and Bipolar transistor models



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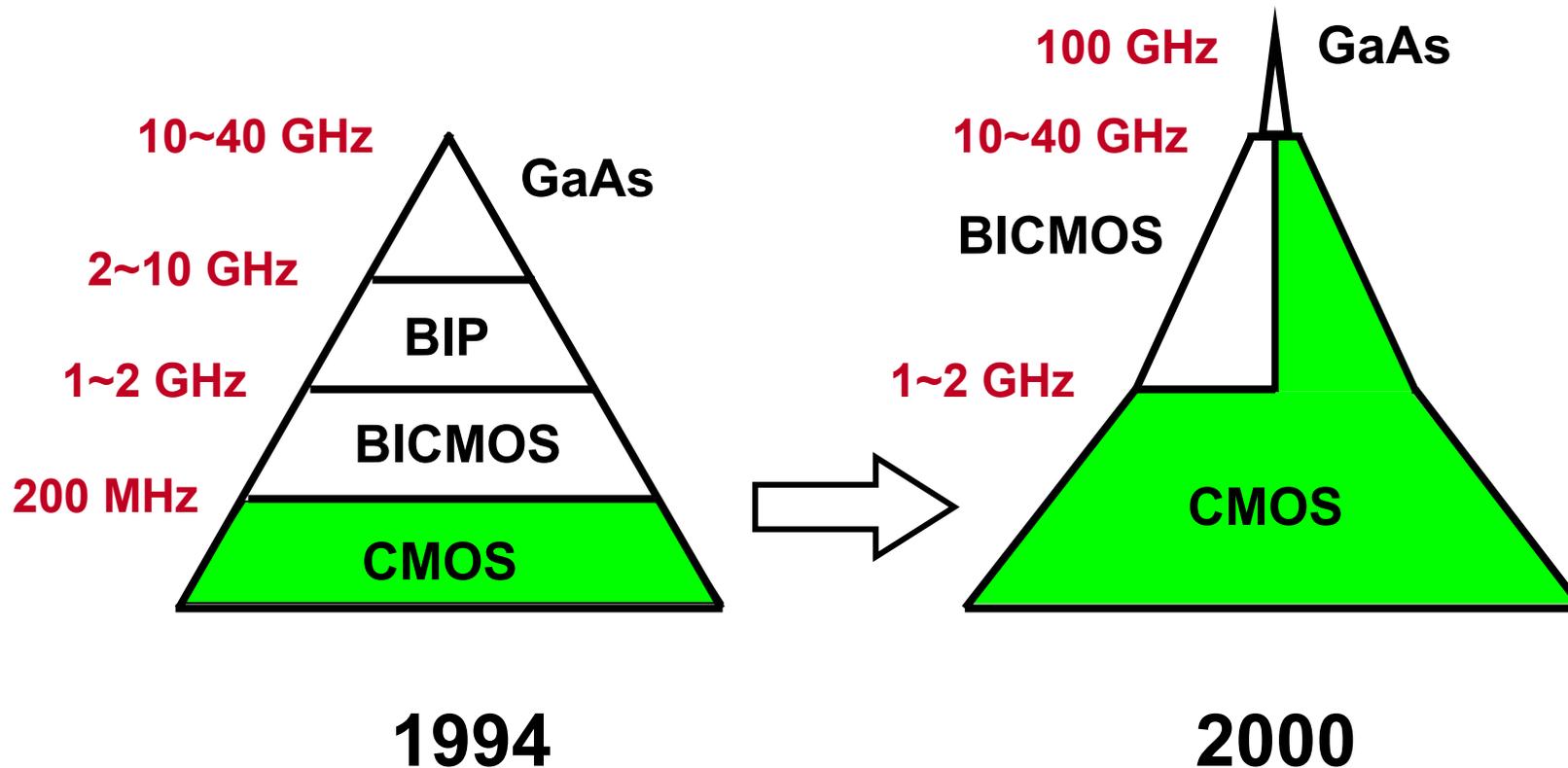


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Ref.: W. Sansen : Analog Design Essentials, Springer 2006

From Bipolar to MOST transistors



Ref.Toshiba

The SIA roadmap

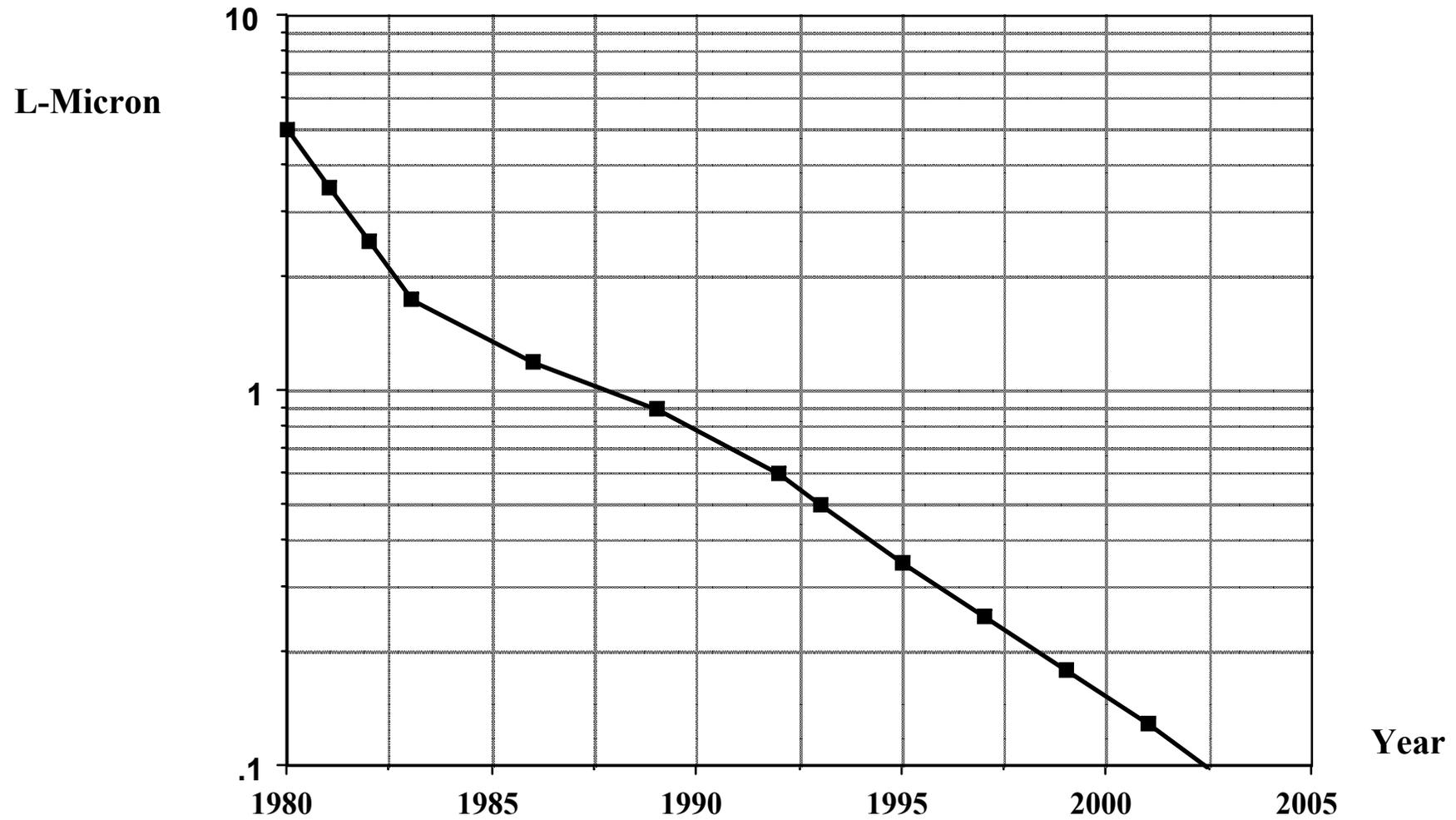
Year	Lmin μm	Bits/chip Gb/chip	Trans/chip millions/chip	Clock MHz	Wiring
1995	0.35	0.064	4	300	4 - 5
1998	0.25	0.256	7	450	5
2001	0.18	1	13	600	5 - 6
2004	0.13	4	25	800	6
2007	0.09	16	50	1000	6 - 7
2010	0.065	64	90	1100	7 - 8

2003

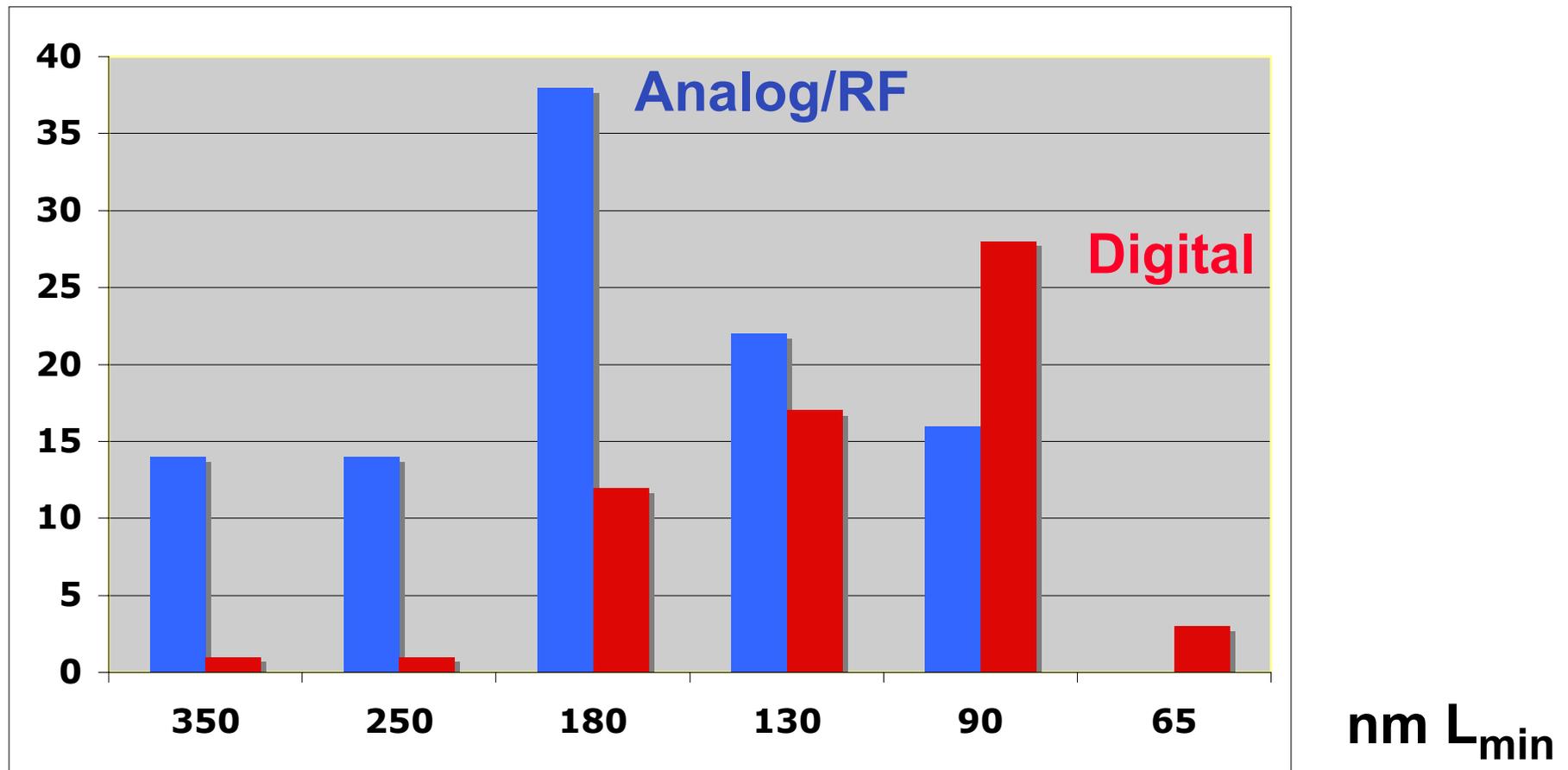


Semiconductor Industry Association

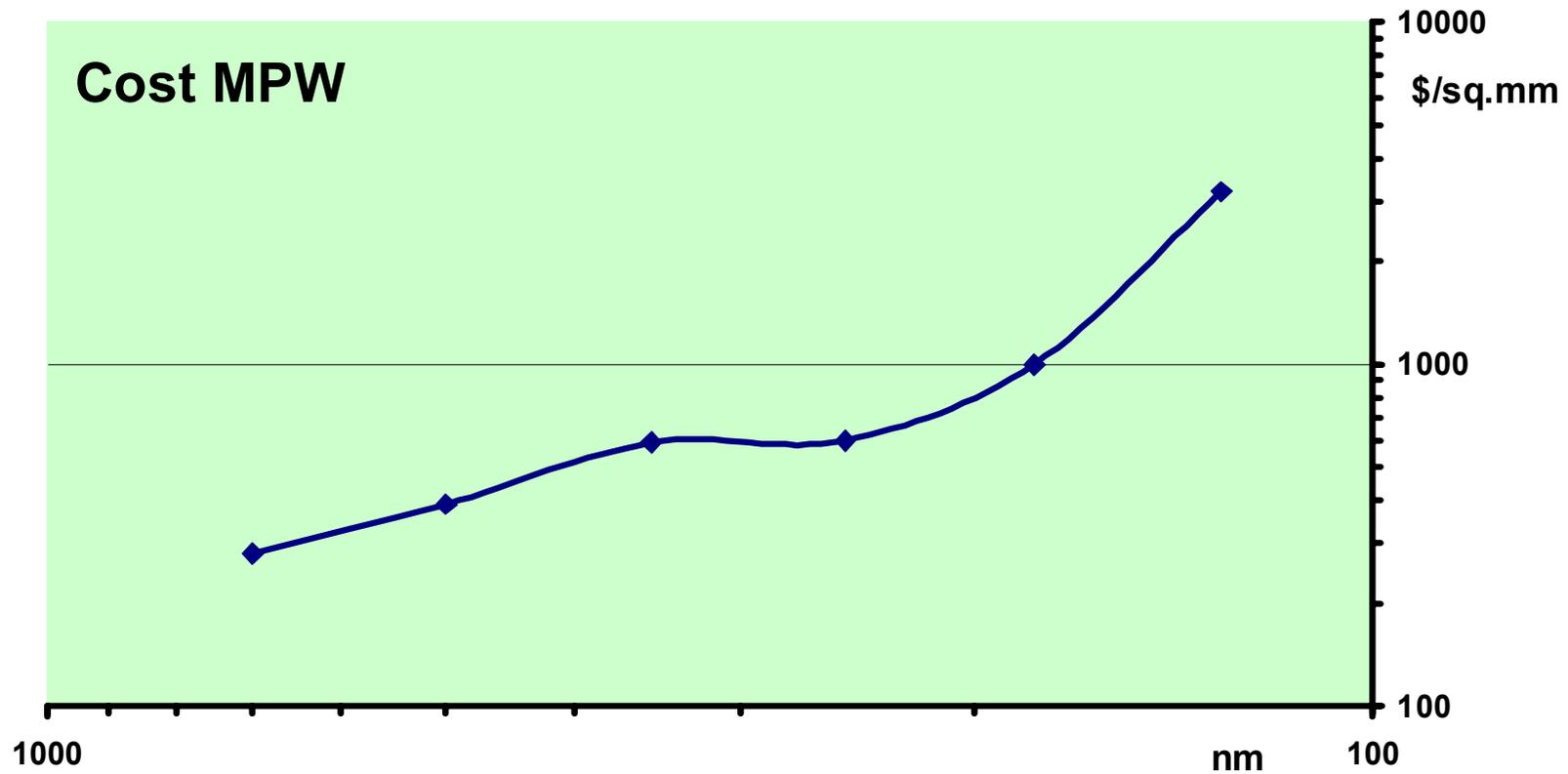
The law of Moore



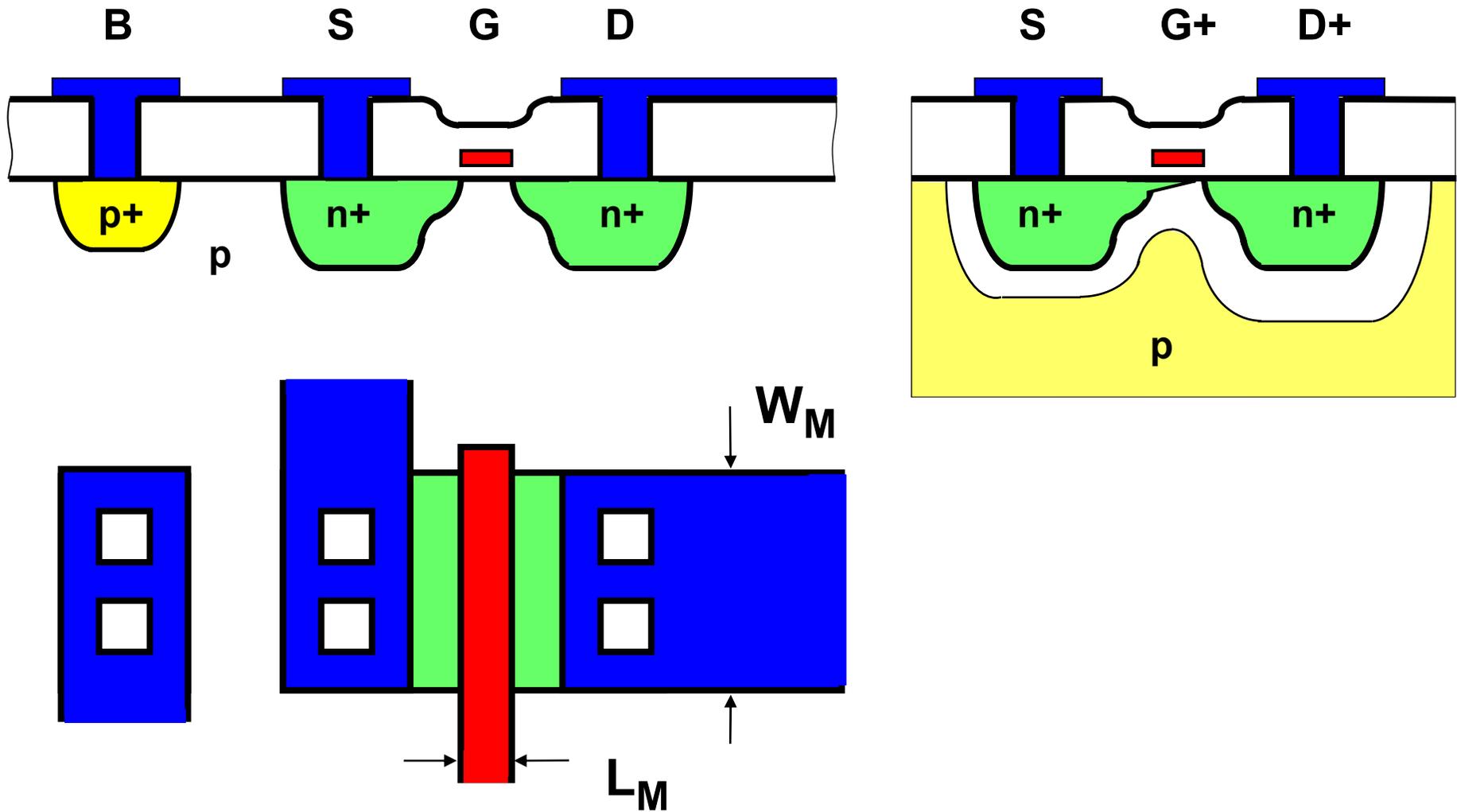
ISSCC 2005 paper distribution



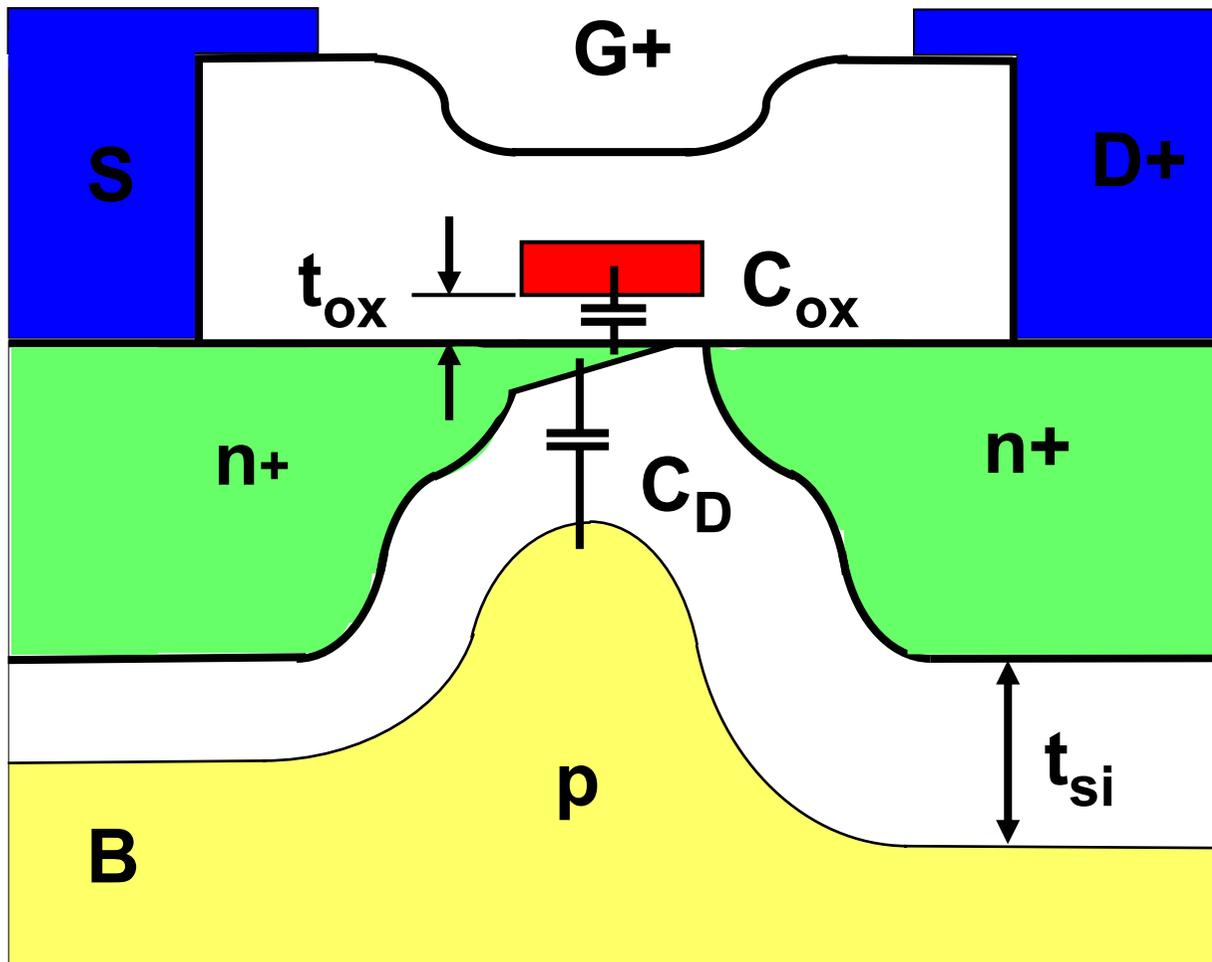
Price MPW silicon for different L (nm)



MOST layout



MOST layout : C_{ox} and C_D



$$C_D = \frac{\epsilon_{si}}{t_{si}}$$

$$C_{ox} = \frac{\epsilon_{ox}}{t_{ox}}$$

$$\frac{C_D}{C_{ox}} = n - 1$$

MOST layout : C_{ox} and C_D values

$$C_D = \frac{\epsilon_{si}}{t_{si}} \quad t_{si} = \sqrt{\frac{2\epsilon_{si}(\phi - V_{BD})}{qN_B}}$$

$$\epsilon_{si} = 1 \text{ pF/cm}$$

$$\epsilon_{ox} = 0.34 \text{ pF/cm}$$

$$\phi \approx 0.6 \text{ V}$$

$$q = 1.6 \cdot 10^{-19} \text{ C}$$

$$N_B \approx 4 \cdot 10^{17} \text{ cm}^{-3}$$

Example : $L = 0.35 \mu\text{m}$; $W/L = 8$

$$V_{BD} = -3.3 \text{ V} : \quad t_{si} = 0.1 \mu\text{m}$$

$$C_D \approx 10^{-7} \text{ F/cm}^2$$

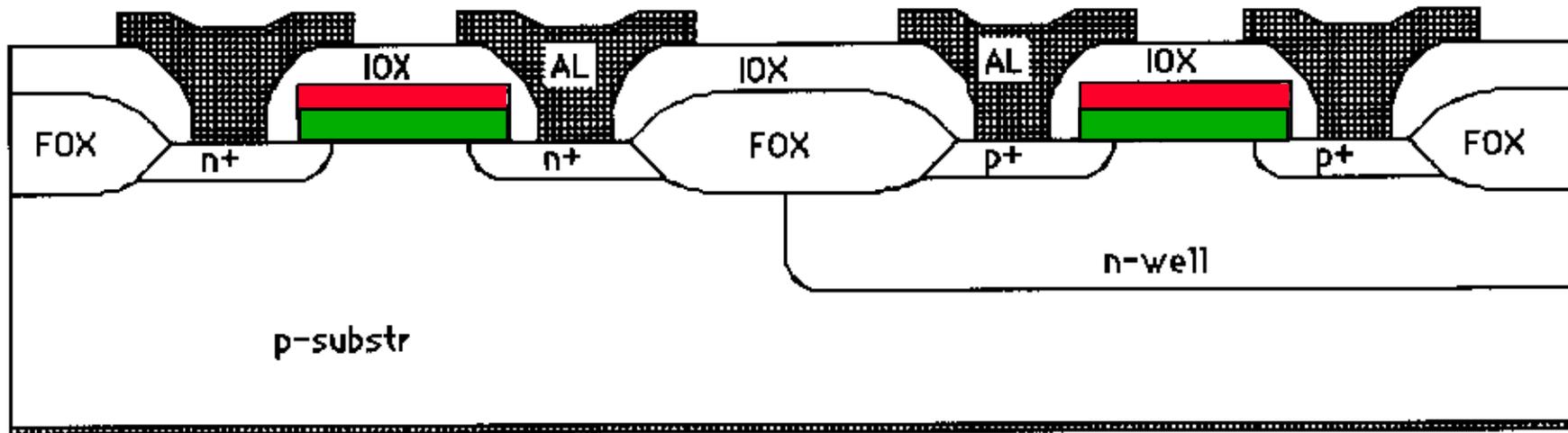
$$t_{ox} = \frac{L_{min}}{50}$$

$$t_{ox} = 7 \text{ nm}$$

$$C_{ox} \approx 5 \cdot 10^{-7} \text{ F/cm}^2$$

$$\frac{C_D}{C_{ox}} = n - 1 \approx 0.2$$

N-well CMOS technology



Gate oxide



Polysilicon gate

MOST I_{DS} versus V_{GS} and V_{DS}

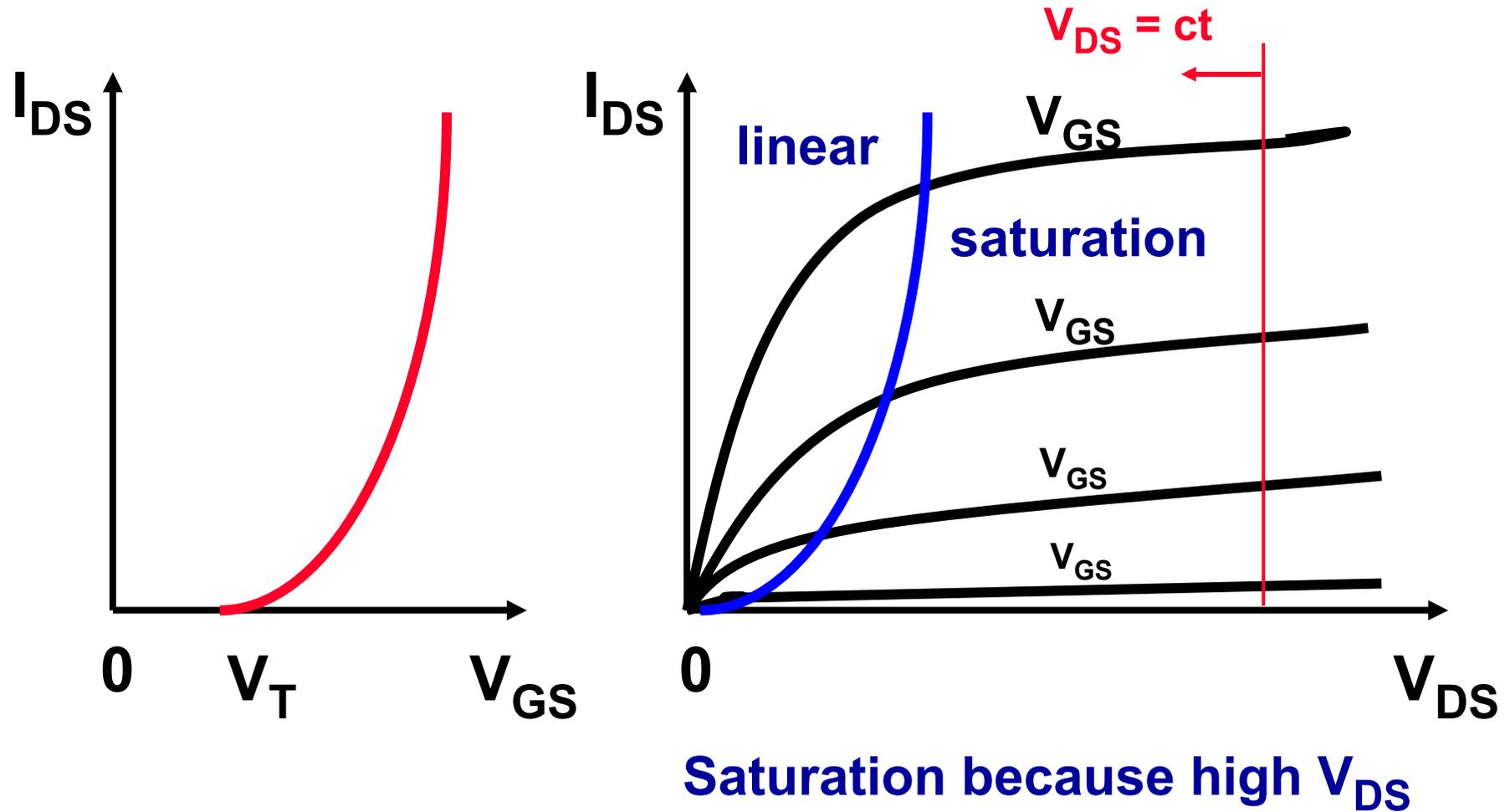
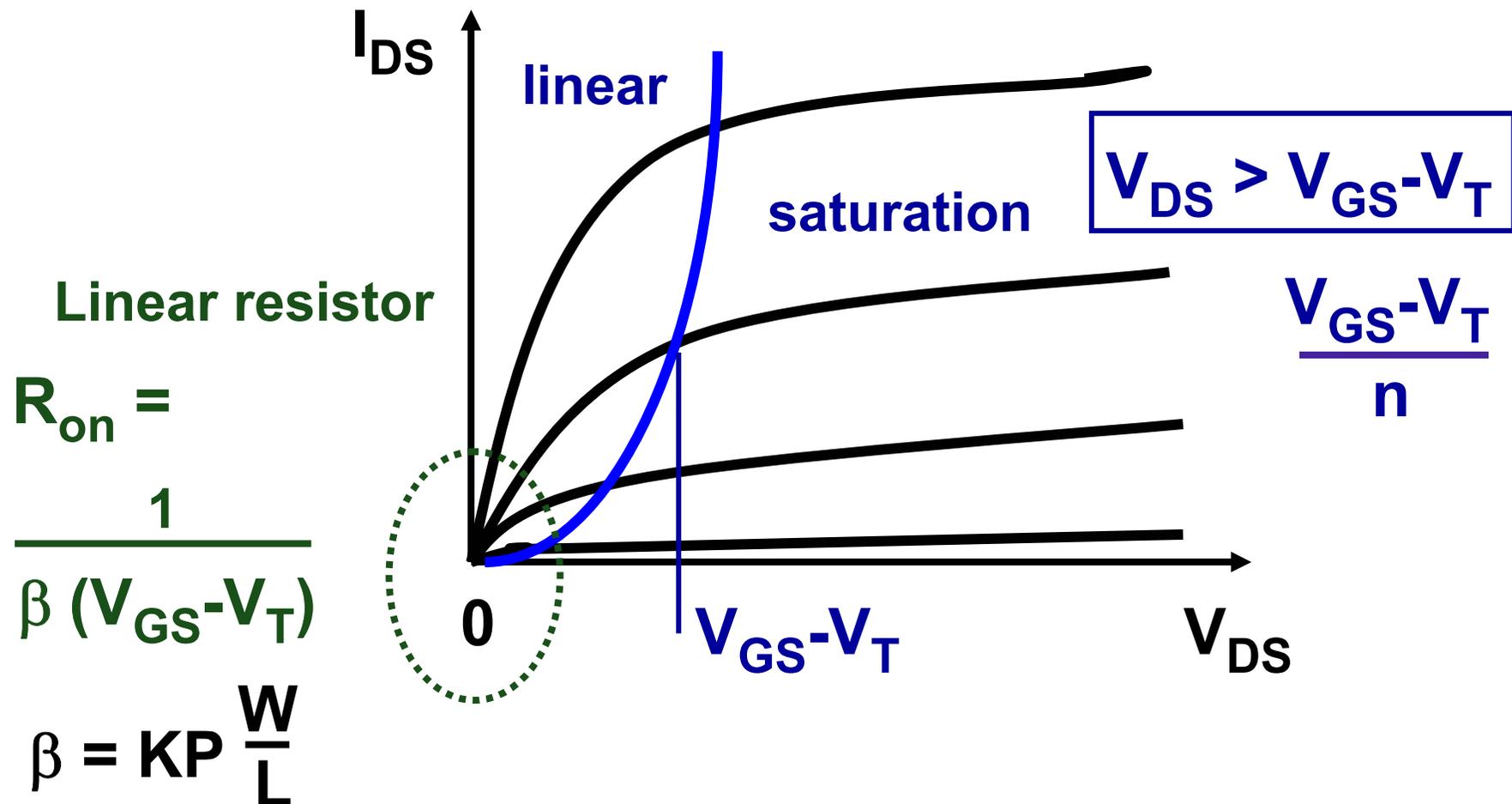


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- **Comparison of MOSTs & Bipolar transistors**

MOST I_{DS} versus V_{DS}



MOST parameters β , KP , C_{ox} , ...

$$\beta = KP \frac{W}{L}$$

$$KP = \mu C_{ox}$$

$$C_{ox} = \frac{\epsilon_{ox}}{t_{ox}}$$

$$t_{ox} = \frac{L_{min}}{50}$$

$$KP_n \approx 300 \mu A/V^2$$

$$C_{ox} \approx 5 \cdot 10^{-7} F/cm^2$$

$$\epsilon_{ox} = 0.34 pF/cm$$

$$\epsilon_{si} = 1 pF/cm$$

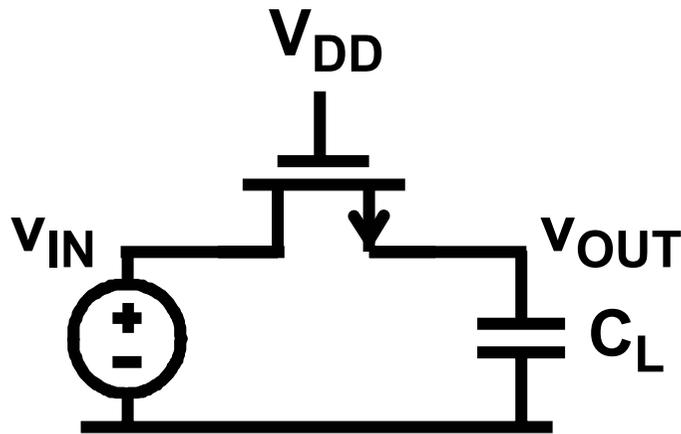
$$t_{ox} = 7 nm$$

$$L_{min} = 0.35 \mu m$$

$$\mu_p \approx 250 cm^2/Vs$$

$$\mu_n \approx 600 cm^2/Vs$$

Example : Analog switch on CL



We want to switch 0.6 V to a load capacitance C_L of 4 pF.

We want to do this fast, with time constant 0.5 ns.

Supply voltage $V_{DD} = 2.5$ V

$V_T = 0.5$ V

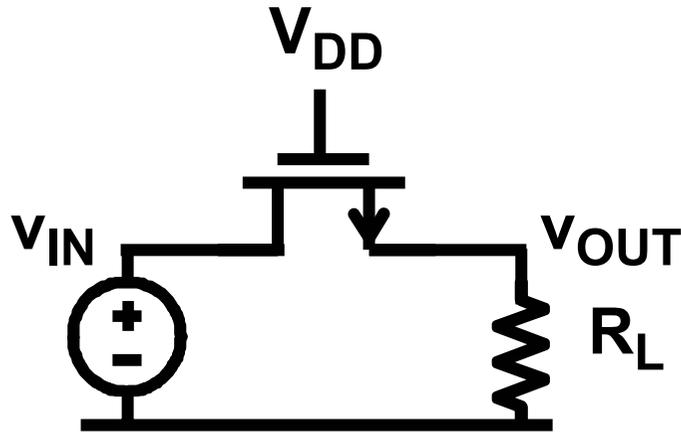
Use standard 0.35 μm CMOS.

Choose

minimum channel length and

find an average V_{GS} !

Example : Analog switch on RL



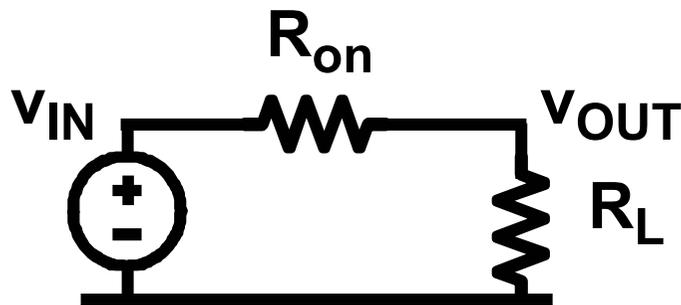
We want to switch 0.6 V to a load resistor R_L of 5 k Ω .

$W/L = 8$

Supply voltage $V_{DD} = 2.5$ V

0.35 μm CMOS: $V_T = 0.5$ V

V_{OUT} ? R_{on} ?



Choose
minimum channel length !

Body effect - Parasitic JFET

$$V_T = V_{T0} + \gamma \left[\sqrt{|2\Phi_F| + V_{BS}} - \sqrt{|2\Phi_F|} \right]$$

$$n = \frac{\gamma}{\sqrt{|2\Phi_F| + V_{BS}}} = 1 + \frac{C_D}{C_{ox}}$$

$$|2\Phi_F| \approx 0.6 \text{ V}$$

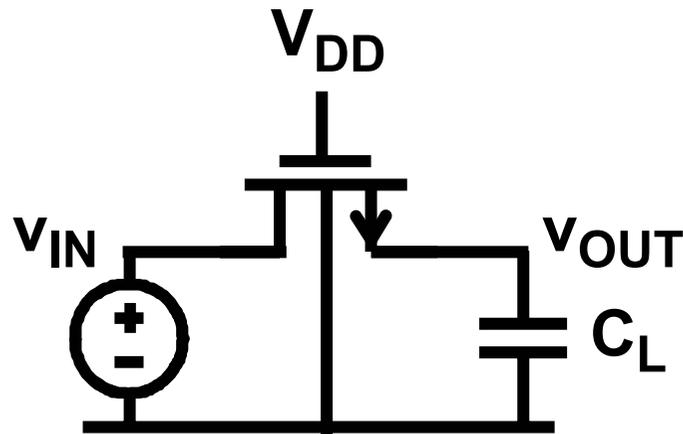
$$n \approx 1.2 \dots 1.5$$

$$\gamma \approx 0.5 \dots 0.8 \text{ V}^{1/2}$$

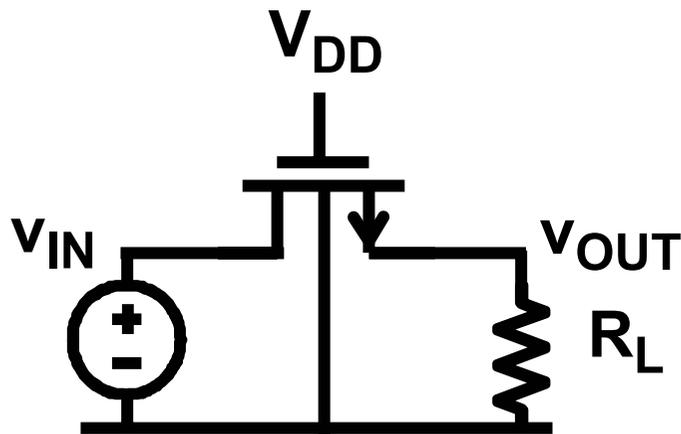
Reverse v_{BS} increases $|V_T|$ and decreases $|i_{DS}|$!!!

$n = 1/\kappa$ subthreshold gate coupling coeff. **Tsividis**

Ex. : Analog switch with nonzero V_{BS}



Switch 0.6 V to a load capacitance C_L of 4 pF or a load resistor R_L of 5 k Ω .
 $W/L = 8$ ($R_{on} = 125 \Omega$ @ $V_{BS} = 0$)
Supply voltage $V_{DD} = 2.5$ V
0.35 μm CMOS: $V_T = 0.5$ V
 $V_{OUT} ?$ for $\gamma = 0.5$ V $^{-1}$

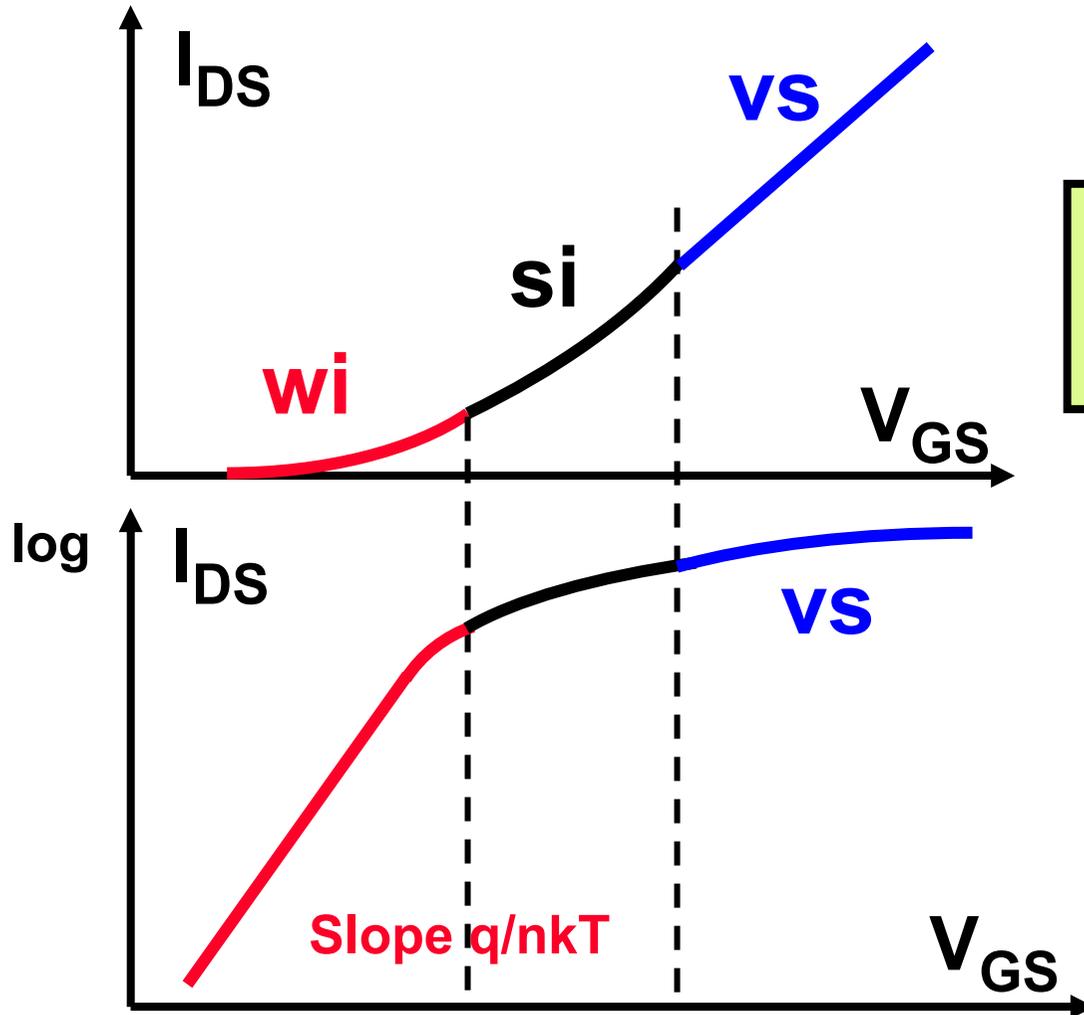


Start with $V_{BS} = 0$.

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MOST I_{DS} versus V_{GS}



$$I_{DS} \sim (V_{GS} - V_T)$$

$$I_{DS} = K'_n \frac{W}{L} (V_{GS} - V_T)^2$$

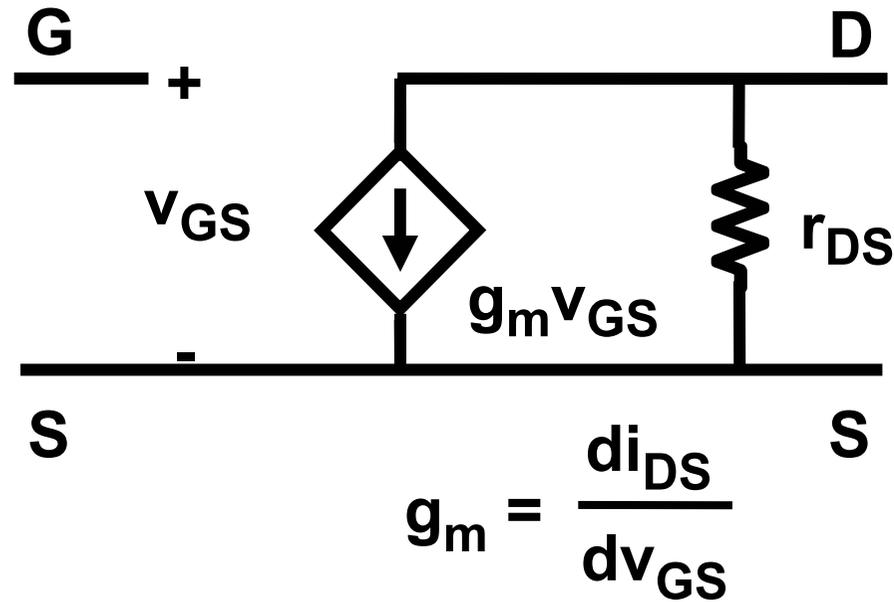
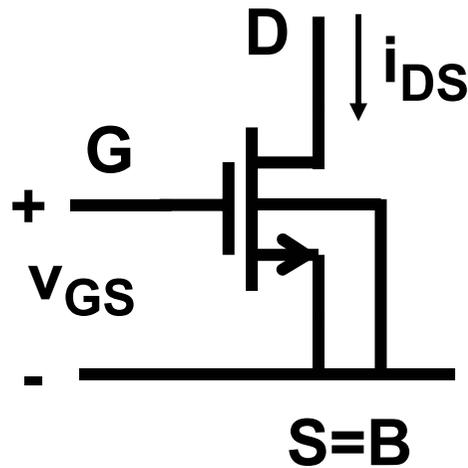
$$K' = \frac{KP}{2n} \quad n = ???$$

$$K'_n \approx 100 \mu\text{A}/\text{V}^2$$

$$K'_p \approx 40 \mu\text{A}/\text{V}^2$$

$$I_{DS} \sim \exp \frac{V_{GS}}{nkT/q}$$

MOST small-signal model : g_m & r_{DS}



$$g_m = 2K'_n \frac{W}{L} (V_{GS} - V_T) = 2 \sqrt{K'_n \frac{W}{L} I_{DS}} = \frac{2 I_{DS}}{V_{GS} - V_T}$$

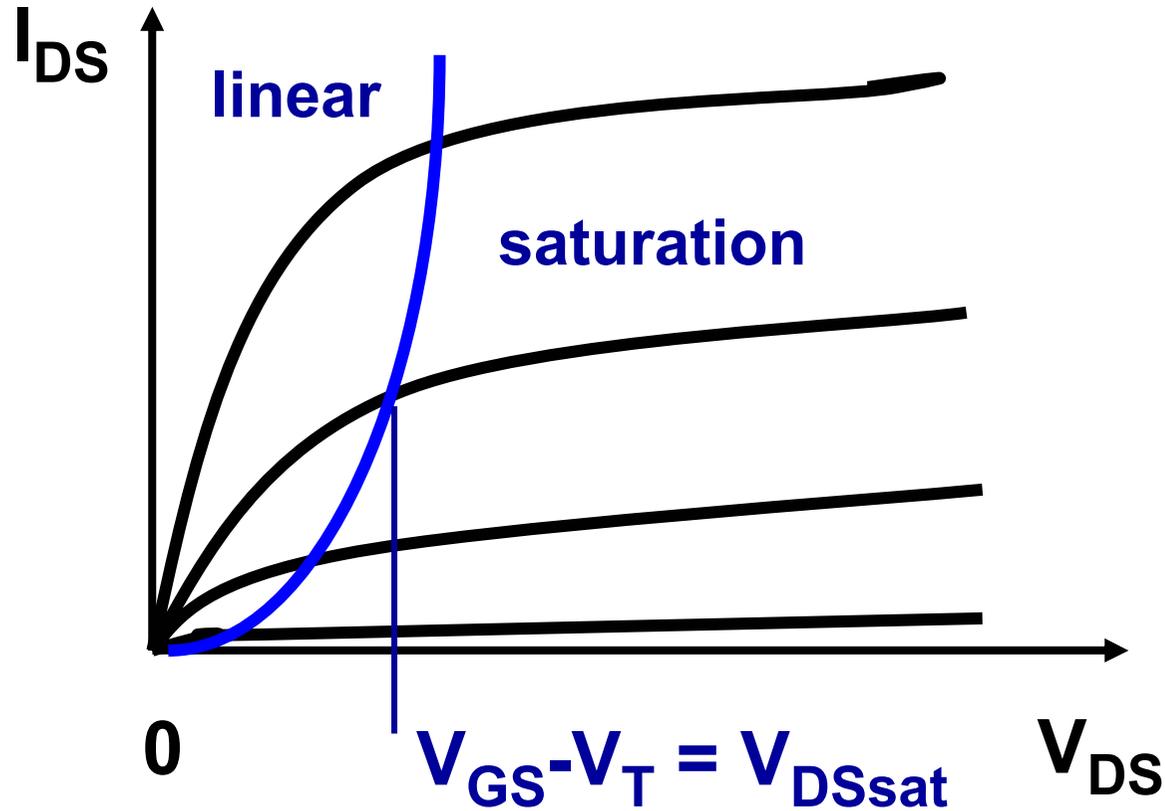
The transconductance g_m

$$\text{Is } g_m \sim \sqrt{I_{DS}}$$

$$\text{or } \sim I_{DS} \quad ?$$



MOST small-signal model : r_{DS}



$$r_{DS} = r_o = \frac{V_{EL}}{I_{DS}}$$

$$\lambda = \frac{1}{V_{EL}}$$

$$V_{En} = 4 \text{ V}/\mu\text{mL}$$

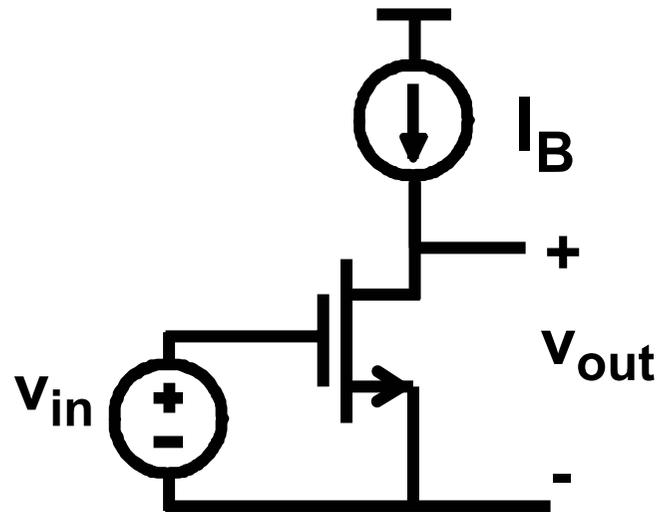
$$L = 1 \mu\text{m}$$

$$I_{DS} = 100 \mu\text{A}$$

$$r_o = 40 \text{ k}\Omega$$

$$I_{DS} = K'_n \frac{W}{L} (V_{GS} - V_T)^2 (1 + \lambda V_{DS})$$

MOST single-transistor gain A_v



$$A_v = g_m r_{DS} = \frac{2 V_E L}{V_{GS} - V_T}$$

$$A_v \approx 100$$

$$\text{If } V_E L \approx 10 \text{ V}$$

$$\text{and } V_{GS} - V_T \approx 0.2 \text{ V}$$

Design for high gain :

	High gain	High speed
$V_{GS}-V_T$	Low (0.2 V)	
L	High	

$V_{GS}-V_T$ sets the ratio g_m/I_{DS} !

Example: single-transistor amplifier

We want to realize a three-stage amplifier with a total gain of 10.000.

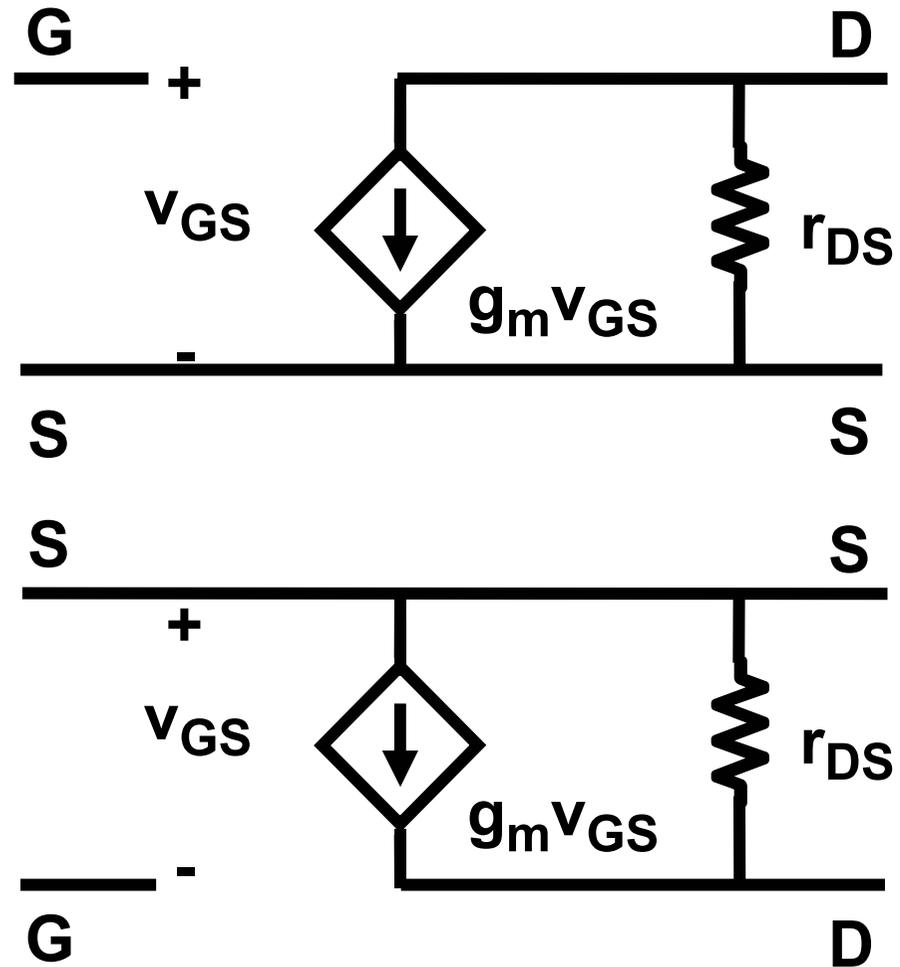
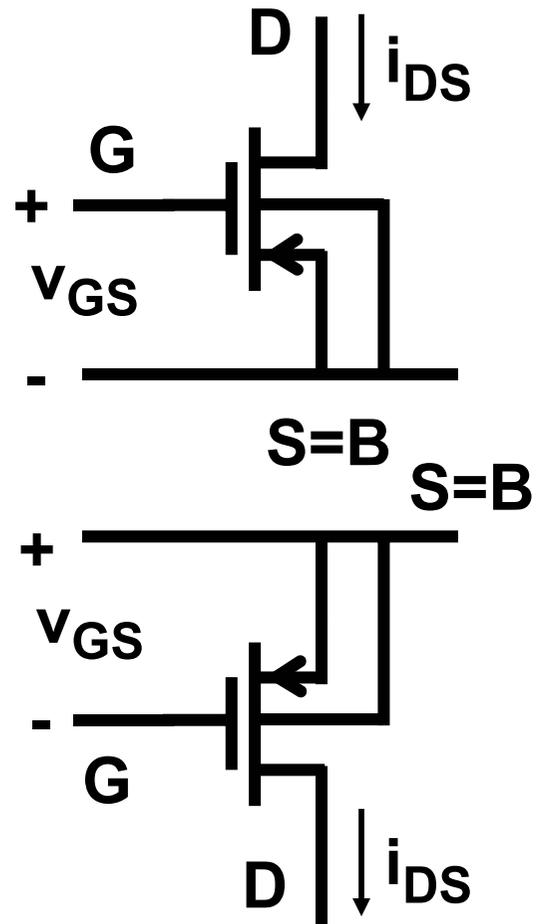
We use three single-transistor stages in series.

What minimum lengths do we have to use in an advanced 65 nm CMOS technology with $V_E = 4 \text{ V}/\mu\text{m}$?

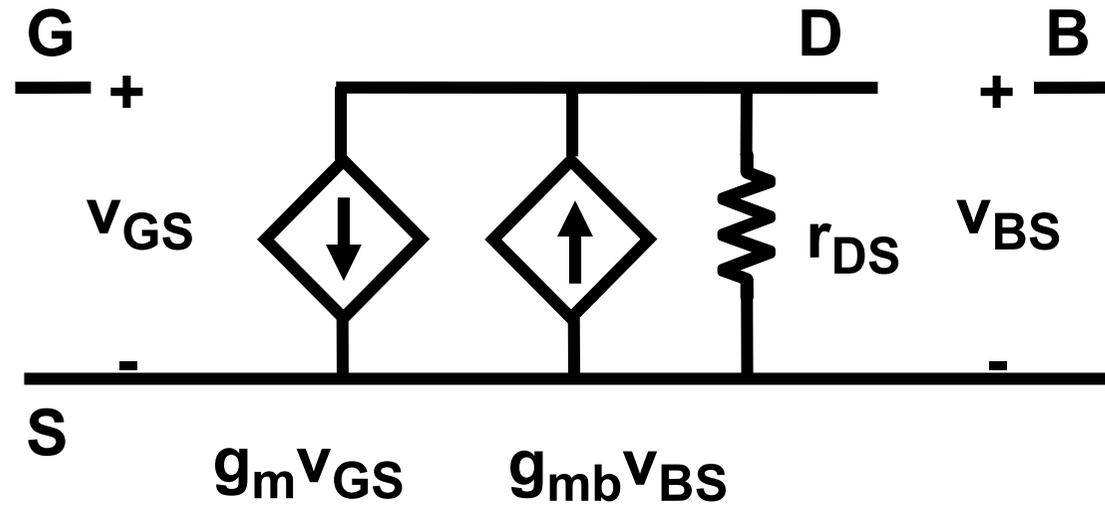
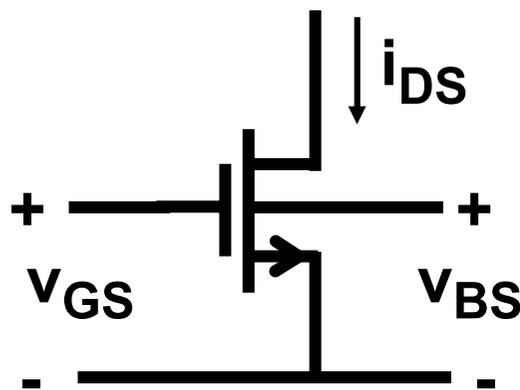
Choose

$$V_{GS} - V_T = 0.2 \text{ V} !$$

pMOST small-signal model



MOST small-signal model: g_m & g_{mb}



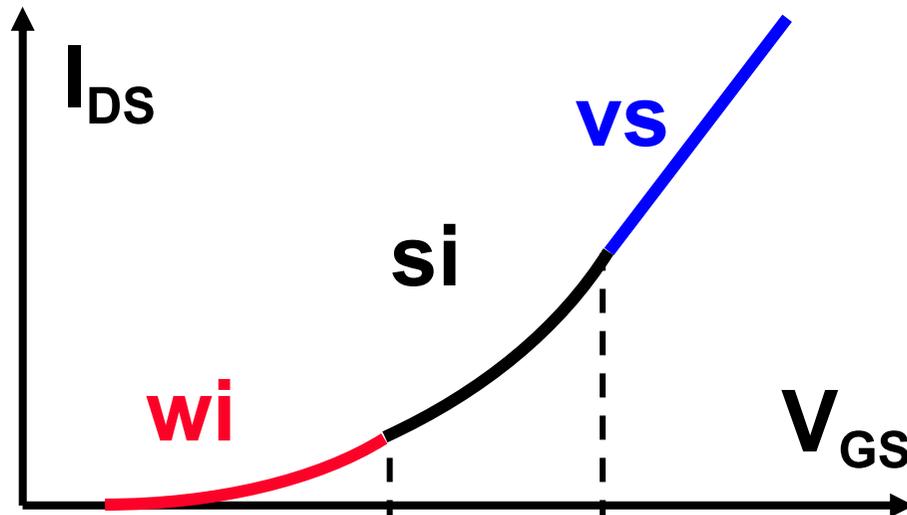
$$g_m = \frac{di_{DS}}{dv_{GS}} \quad g_{mb} = \frac{di_{DS}}{dv_{BS}}$$

$$\frac{g_{mb}}{g_m} = \frac{C_D}{C_{ox}} = n - 1$$

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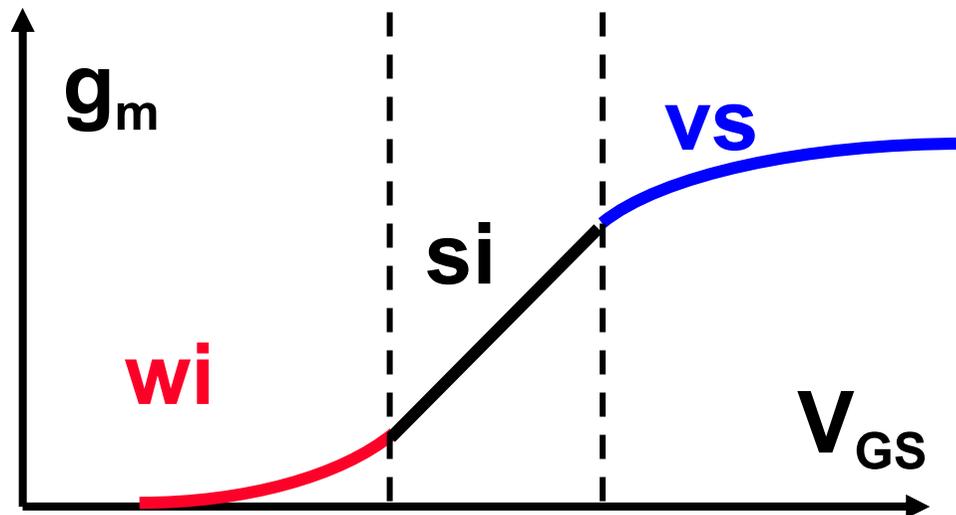
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I_{DS} & g_m versus V_{GS} : weak inversion



wi : weak inversion

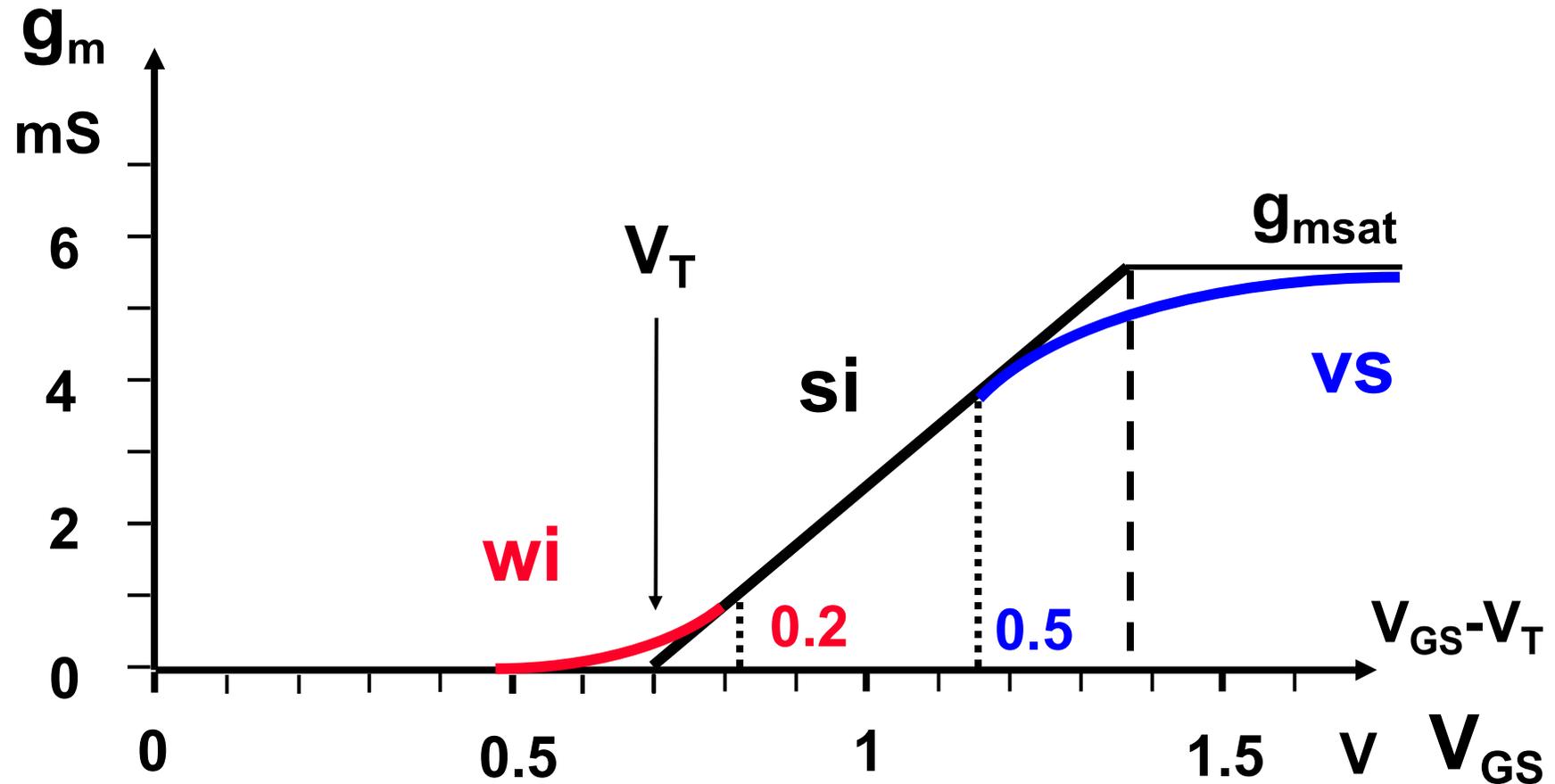
$$I_{DSwi} = I_{D0} \frac{W}{L} \exp \frac{V_{GS}}{nkT/q}$$



Subthreshold slope :
 $nkT/q \ln(10)$

$$g_{mwi} = \frac{I_{DSwi}}{nkT/q}$$

Transconductance g_m versus V_{GS}



Transition voltage V_{GS_t} between wi & si

$$I_{DSwi} = I_{D0} \frac{W}{L} \exp^{\frac{V_{GS}}{nkT/q}}$$

$$g_{mwi} = \frac{I_{DSwi}}{nkT/q}$$

$$\frac{g_{mwi}}{I_{DSwi}} = \frac{1}{nkT/q}$$

$$I_{DS} = K'_n \frac{W}{L} (V_{GS} - V_T)^2$$

$$g_m = \frac{2 I_{DS}}{V_{GS} - V_T}$$

$$\frac{g_m}{I_{DS}} = \frac{2}{V_{GS} - V_T}$$

$$(V_{GS_t} - V_T)_t = 2n \frac{kT}{q}$$

Transition Voltage V_{GSt} for different L

$$(V_{GSt} - V_T)_t = 2n \frac{kT}{q}$$

$$I_{DSt} \approx K'_n \frac{W}{L} \left(2n \frac{kT}{q}\right)^2$$

Is independent of channel length L

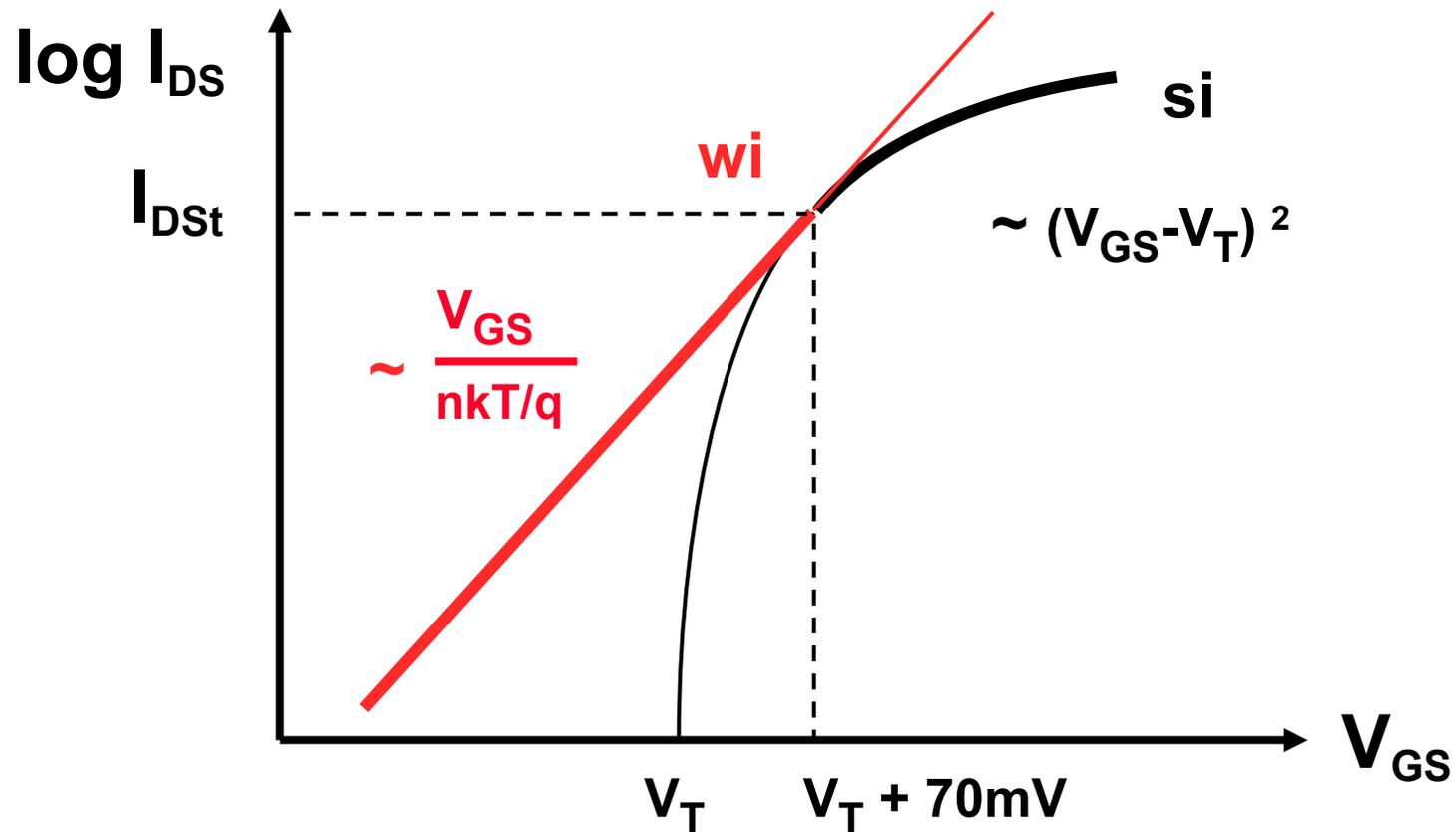
Is still true in ... years !

$$(V_{GSt} - V_T)_t = 2n \frac{kT}{q} \approx 70 \text{ mV}$$

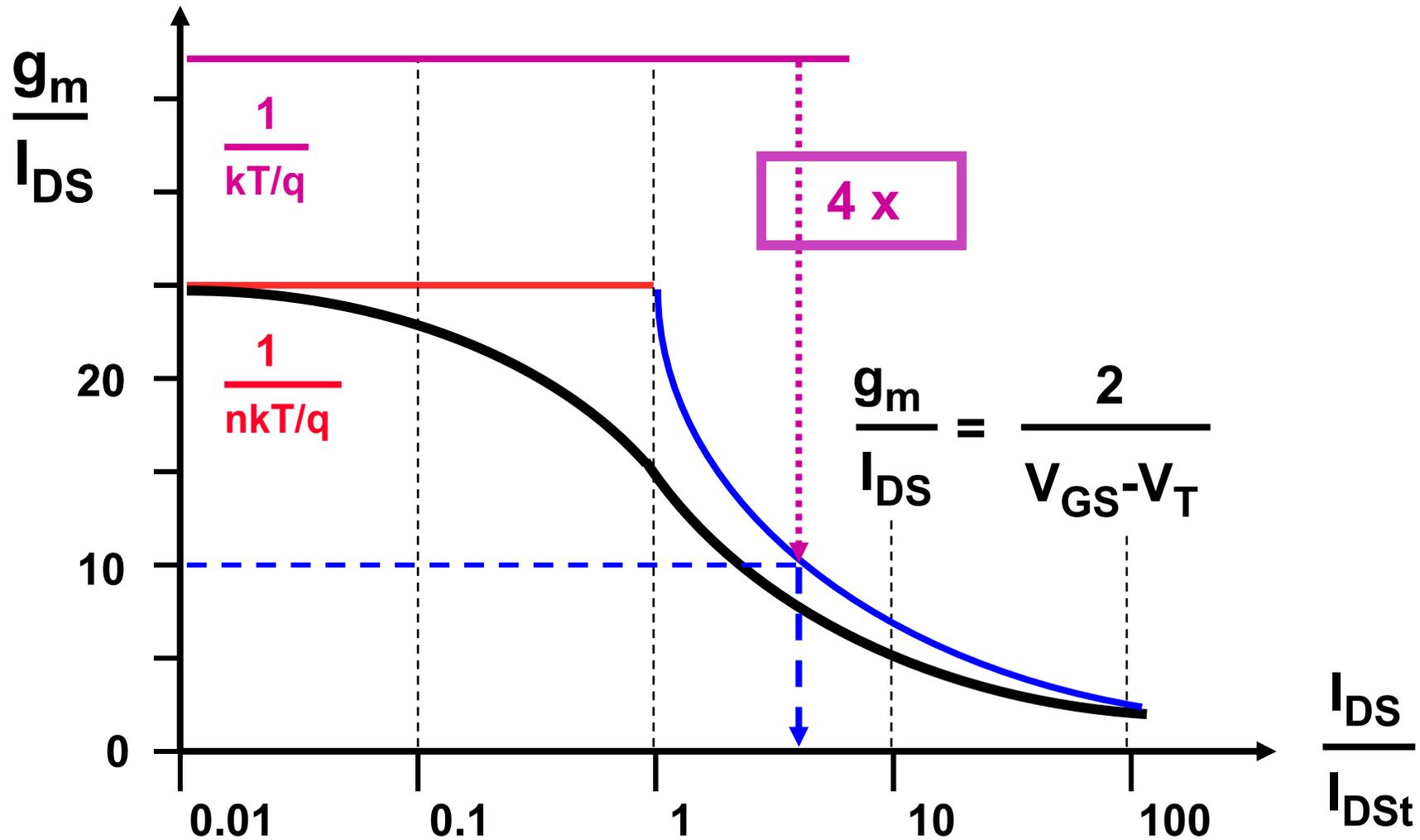
$$I_{DSt} \approx 2 \mu\text{A for } \frac{W}{L} = 10$$

for nMOST

Transition wi - si



Ratio g_m/I_{DS} at the transition wi - si



EKV model for smooth wi-si transition

$$I_{DS} = K' \frac{W}{L} V_{GSTt}^2 [\ln(1 + e^v)]^2 \quad V_{GST} = V_{GS} - V_T \quad K' = \frac{KP}{2n}$$

$$v = \frac{V_{GST}}{V_{GSTt}} \quad V_{GSTt} = (V_{GS} - V_T)_t = 2n \frac{kT}{q}$$

≈ 70 mV

Small v : $\ln(1 + e^v) \approx e^v$

$$I_{DS} = K' \frac{W}{L} V_{GSTt}^2 e^{2v} = \underbrace{K' \frac{W}{L} V_{GSTt}^2}_{I_{DSt}} \exp\left(\frac{V_{GS} - V_T}{n kT/q}\right)$$

Large v : $\ln(1 + e^v) \approx v$

$$I_{DS} = K' \frac{W}{L} V_{GSTt}^2 v^2 = K' \frac{W}{L} (V_{GS} - V_T)^2$$

Enz, AICSP '95,
83-114

Cunha, JSSC Oct.98
1510-1519

Transition current I_{DSt} between w_i & s_i

$$I_{DSt} = I_{DS} \left| \begin{array}{l} = K' \frac{W}{L} V_{GSTt}^2 \\ V = 1 \\ i = 1 \end{array} \right.$$

$$I_{DSt} = 2 \mu A \text{ for } W/L = 10$$

$$i = \frac{I_{DS}}{I_{DSt}} = [\ln (1 + e^v)]^2 \quad \text{inversion coefficient}$$

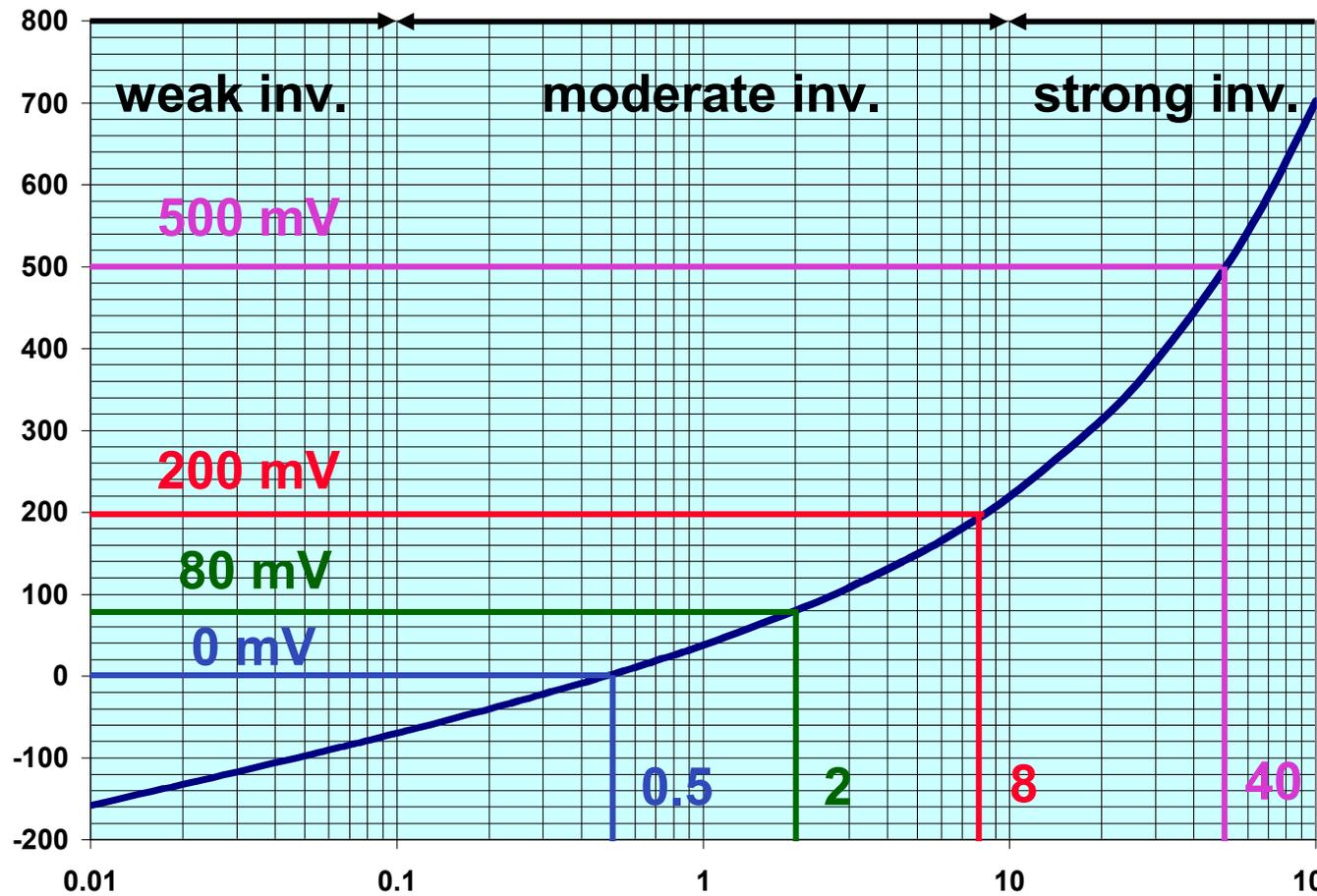
$$v = \ln (e^{\sqrt{i}} - 1)$$

$$V_{GS} - V_T = V_{GSTt} \ln (e^{\sqrt{i}} - 1)$$

$$V_{GSTt} = 2n \frac{kT}{q} \approx 70 \text{ mV}$$

Relation $V_{GS}-V_T$ and inversion coefficient i

$V_{GS}-V_T$ (mV)



$$V_{GS}-V_T =$$

$$V_{GSTt} \ln(e^{\sqrt{i}} - 1)$$

$$V_{GSTt} = 2n \frac{kT}{q}$$

$$i = \frac{I_{DS}}{I_{DSt}}$$

Transconductance g_m between w_i & s_i

$$i = \frac{I_{DS}}{I_{DSt}} = [\ln(1 + e^v)]^2 \quad g_m \approx \dots$$

$$GM = \frac{g_m}{I_{DS}} \frac{nkT}{q} = \frac{1 - e^{-\sqrt{i}}}{\sqrt{i}}$$

$$\text{Large } i : GM = \frac{1}{\sqrt{i}}$$

$$\text{Small } i : GM = 1 - \frac{\sqrt{i}}{2}$$

Alternative approximation :

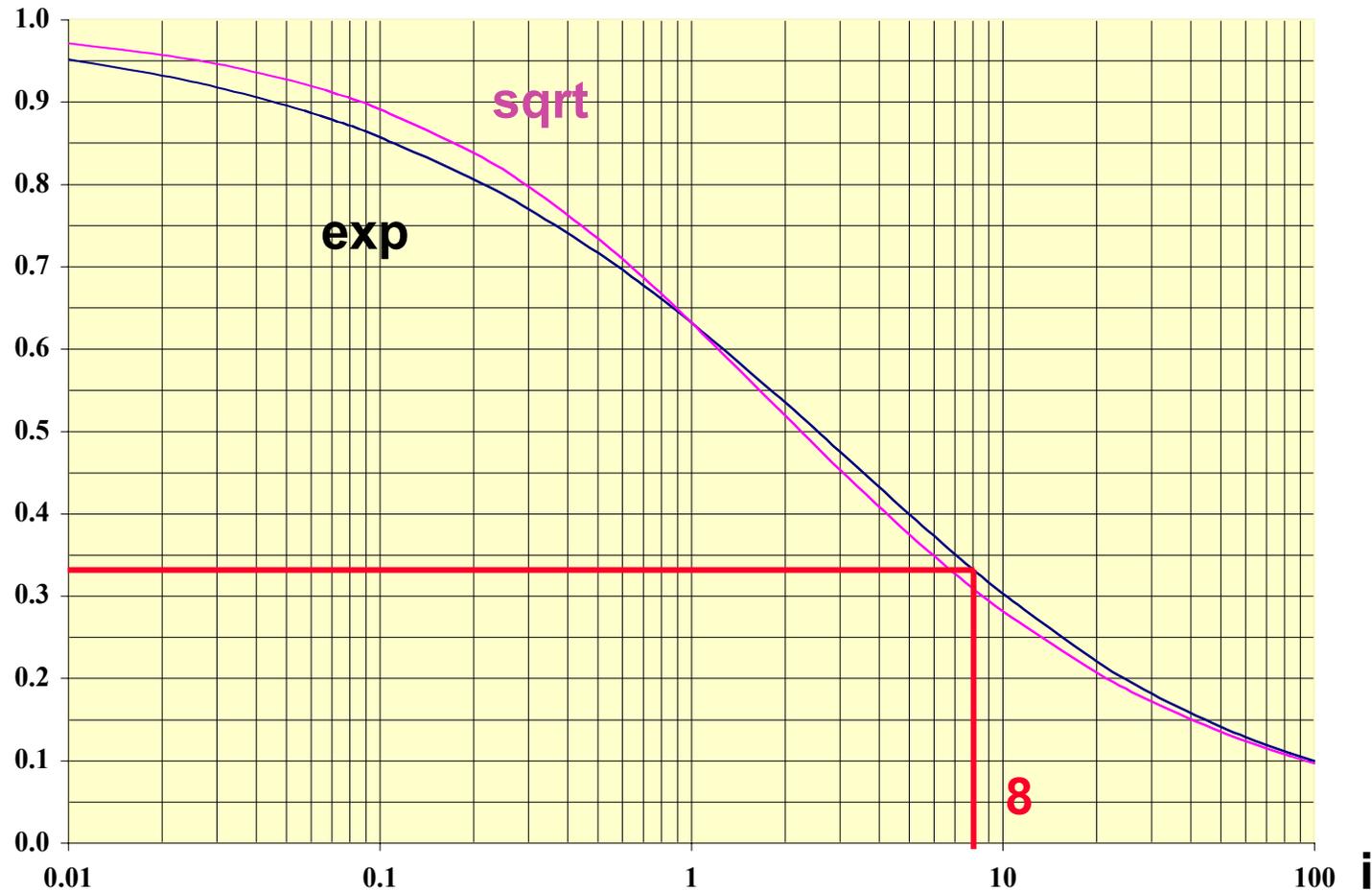
$$GM = \frac{1}{\sqrt{1 + 0.5\sqrt{i} + i}}$$

$$\text{Large } i : GM = \frac{1}{\sqrt{i}}$$

$$\text{Small } i : GM = 1 - \frac{\sqrt{i}}{4}$$

GM versus inversion coefficient i

GM



$$GM = \frac{g_m}{I_{DS}} \frac{nkT}{q}$$

GM =

$$\frac{1 - e^{-\sqrt{i}}}{\sqrt{i}}$$

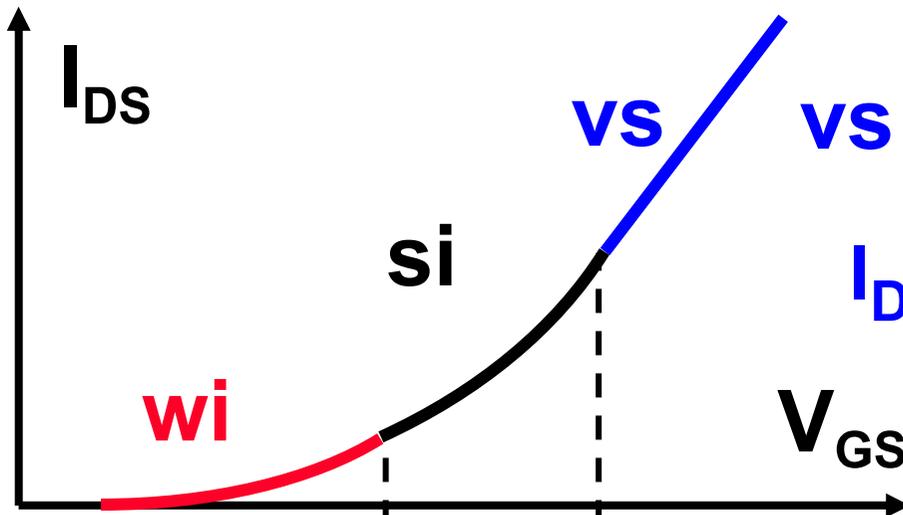
$$\frac{1}{\sqrt{1 + 0.5\sqrt{i} + i}}$$

$$i = \frac{I_{DS}}{I_{DSst}}$$

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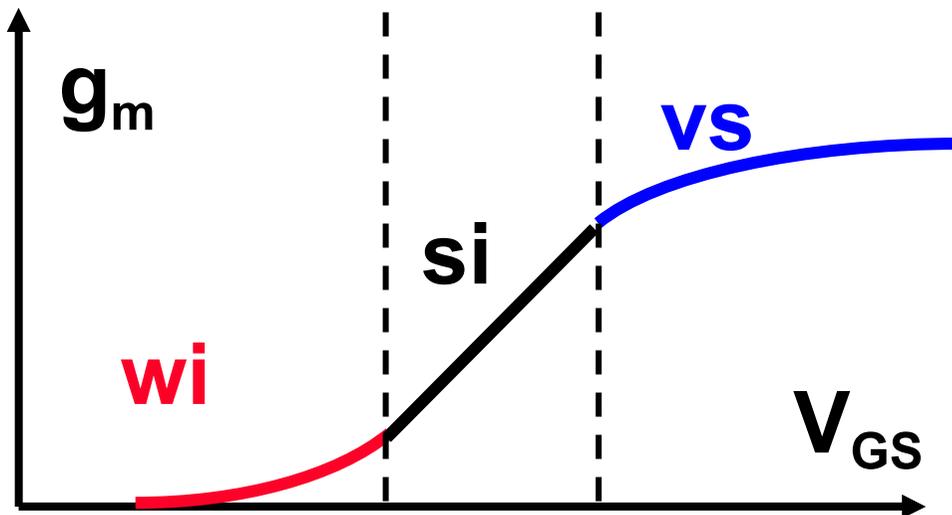
I_{DS} & g_m vs V_{GS} : velocity saturation



vs : velocity saturation

$$I_{DSvs} = WC_{ox}v_{sat}(V_{GS}-V_T)$$

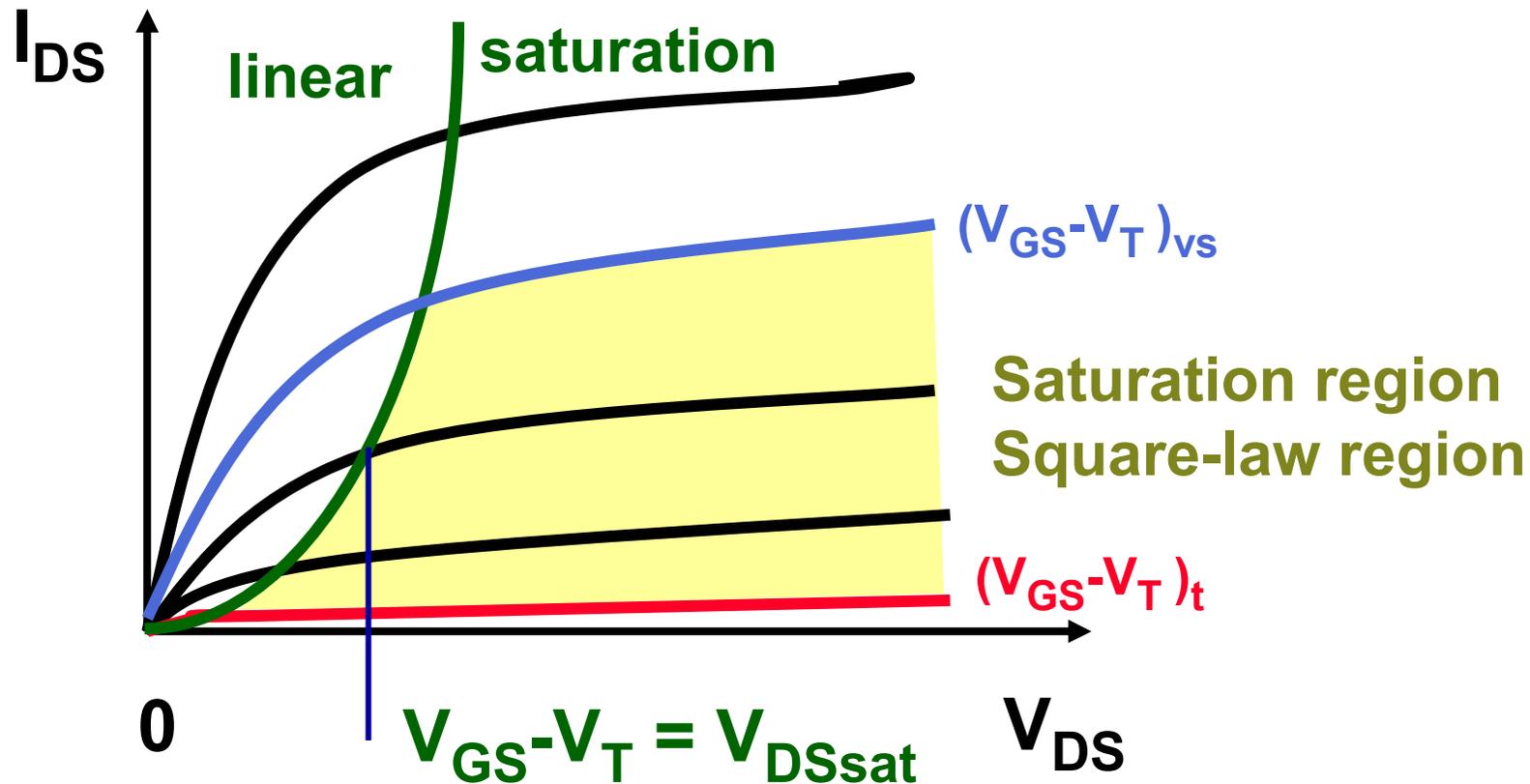
$$v_{sat} \approx 10^7 \text{ cm/s}$$



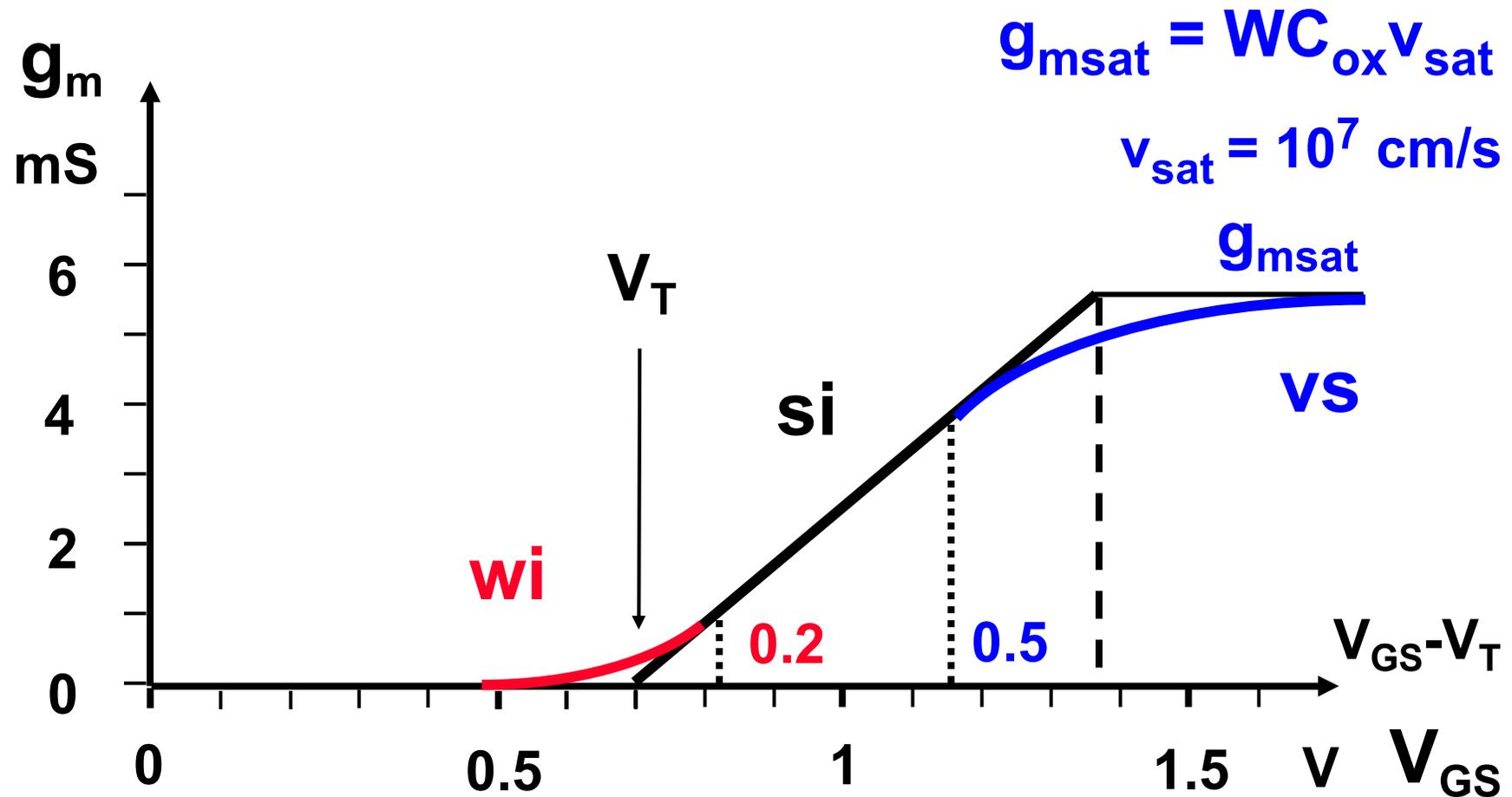
$$g_{msat} = WC_{ox}v_{sat}$$

is absolute max. !

The saturation region and velocity saturation



Transconductance g_m versus V_{GS}



Velocity saturation : v_{sat} & θ

$$I_{\text{DS}} = \frac{K'_n \frac{W}{L} (V_{\text{GS}} - V_{\text{T}})^2}{1 + \theta (V_{\text{GS}} - V_{\text{T}})}$$

[large V_{GS}]

$$\approx \frac{K'_n W}{\theta L} (V_{\text{GS}} - V_{\text{T}})$$

$$g_{\text{msat}} \approx 2K'_n \frac{W}{L} (V_{\text{GS}} - V_{\text{T}})^2 \frac{1 + \frac{\theta}{2}(V_{\text{GS}} - V_{\text{T}})}{[1 + \theta (V_{\text{GS}} - V_{\text{T}})]^2} \approx \frac{K'_n W}{\theta L}$$

$$= WC_{\text{ox}} v_{\text{sat}}$$

$$\boxed{\theta L = \frac{\mu}{2n} \frac{1}{v_{\text{sat}}}} = \frac{1}{E_{\text{c}}} \quad E_{\text{c}} \text{ is the vertical critical field !}$$

$$\theta L \approx 0.2 \mu\text{m/V} : \text{ For } L = 0.13 \mu\text{m} \quad \theta \approx 1.6 \text{ V}^{-1}$$

Velocity saturation : θ & R_S & v_{sat}

$$I_{DS} = \frac{K'_n \frac{W}{L} (V_{GS} - V_T)^2}{1 + \theta (V_{GS} - V_T)}$$

[large V_{GS}]

$$g_{msat} \approx \frac{K'_n}{\theta} \frac{W}{L}$$

$$g_m R_S = \frac{g_m}{1 + g_m R_S} \approx \frac{1}{R_S}$$

$$R_S = \frac{\theta}{K'_n W/L}$$

$$R_S \approx \frac{\mu}{2n} \frac{1}{W K'_n v_{sat}} \approx \frac{1}{W C_{ox} v_{sat}}$$

Transition Voltage $V_{GS} - V_T$ between i_D and v_s

$$I_{DS} = \frac{K'_n \frac{W}{L} (V_{GS} - V_T)^2}{1 + \theta (V_{GS} - V_T)}$$

$$I_{DSsat} = WC_{ox} v_{sat} (V_{GS} - V_T)$$

$$g_{msat} = WC_{ox} v_{sat} \approx \frac{K'_n}{\theta} \frac{W}{L}$$

$$(V_{GS} - V_T)_{vs} = \frac{1}{\theta} \approx 2nL \frac{v_{sat}}{\mu}$$

Is proportional to channel length L !!!

$$\approx 5 L \approx 0.62 \text{ V if } L = 0.13 \mu\text{m}$$

Transition Current I_{DSvs} between si and vs

$$I_{DSvs} \approx K' WL \left(\frac{2n v_{sat}}{\mu} \right)^2 \approx 100 n \epsilon_{ox} W \frac{v_{sat}^2}{\mu}$$

$$\frac{I_{DSvs}}{W} \approx 10 \text{ A/cm}$$

$$K' = \frac{\mu C_{ox}}{2n}$$

$$C_{ox} = \frac{\epsilon_{ox}}{t_{ox}} \quad t_{ox} = \frac{L}{50}$$

$W = 2.6 \mu\text{m}$ & $L = 0.13 \mu\text{m}$:

$I_{DSvs} \approx 2.6 \text{ mA}$

$v_{sat} = 10^7 \text{ cm/s}$

$n = 1.4$

$\mu = 500 \text{ cm}^2/\text{Vs}$

Transconductance g_m between i and v_s

$$g_{msat} = W C_{ox} v_{sat}$$

$$g_{msat} \approx 17 \cdot 10^{-5} W/L \text{ S/cm}$$

$$g_{mK'} = 2K' \frac{W}{L} \underbrace{(V_{GS} - V_T)}_{V_{GST}}$$

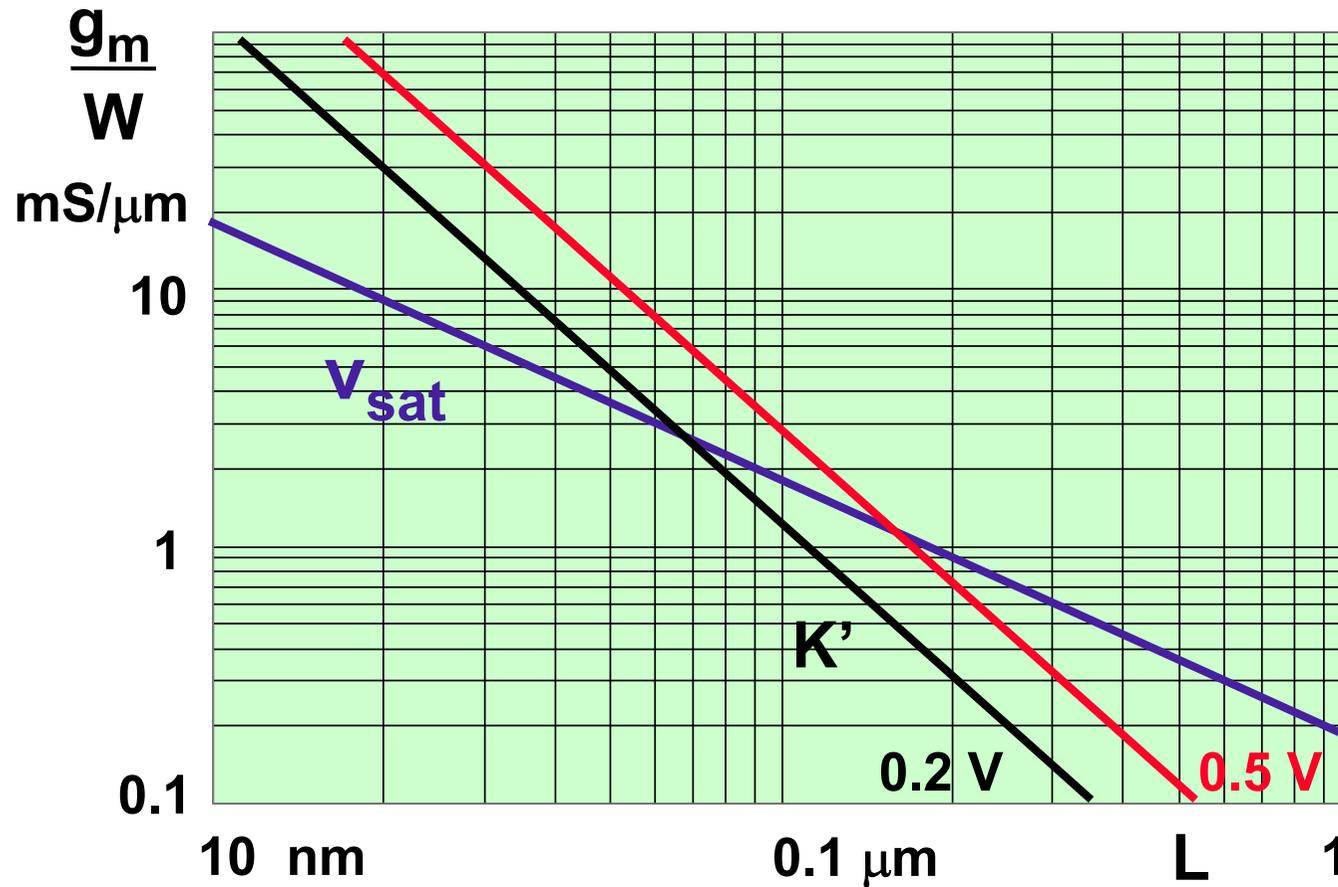
$$g_{mK'} \approx 1.2 \cdot 10^{-9} V_{GST} W/L^2 \text{ S/cm}$$

$$\frac{1}{g_m} = \frac{1}{g_{mK'}} + \frac{1}{g_{msat}}$$

$$g_m \approx \frac{W}{L} \frac{17 \cdot 10^{-5}}{1 + 2.8 \cdot 10^4 L / V_{GST}} \quad L \text{ in cm}$$

If $V_{GST} = 0.2 \text{ V}$, v_{sat} takes over for $L < 65 \text{ nm}$ (If 0.5 V for $L < 0.15 \mu\text{m}$)

Now in velocity saturation ?



$$V_{GS} - V_T \approx 0.2 V$$

(0.5 V)

$$\frac{g_m}{W} = \frac{2K'}{L} (V_{GS} - V_T)$$

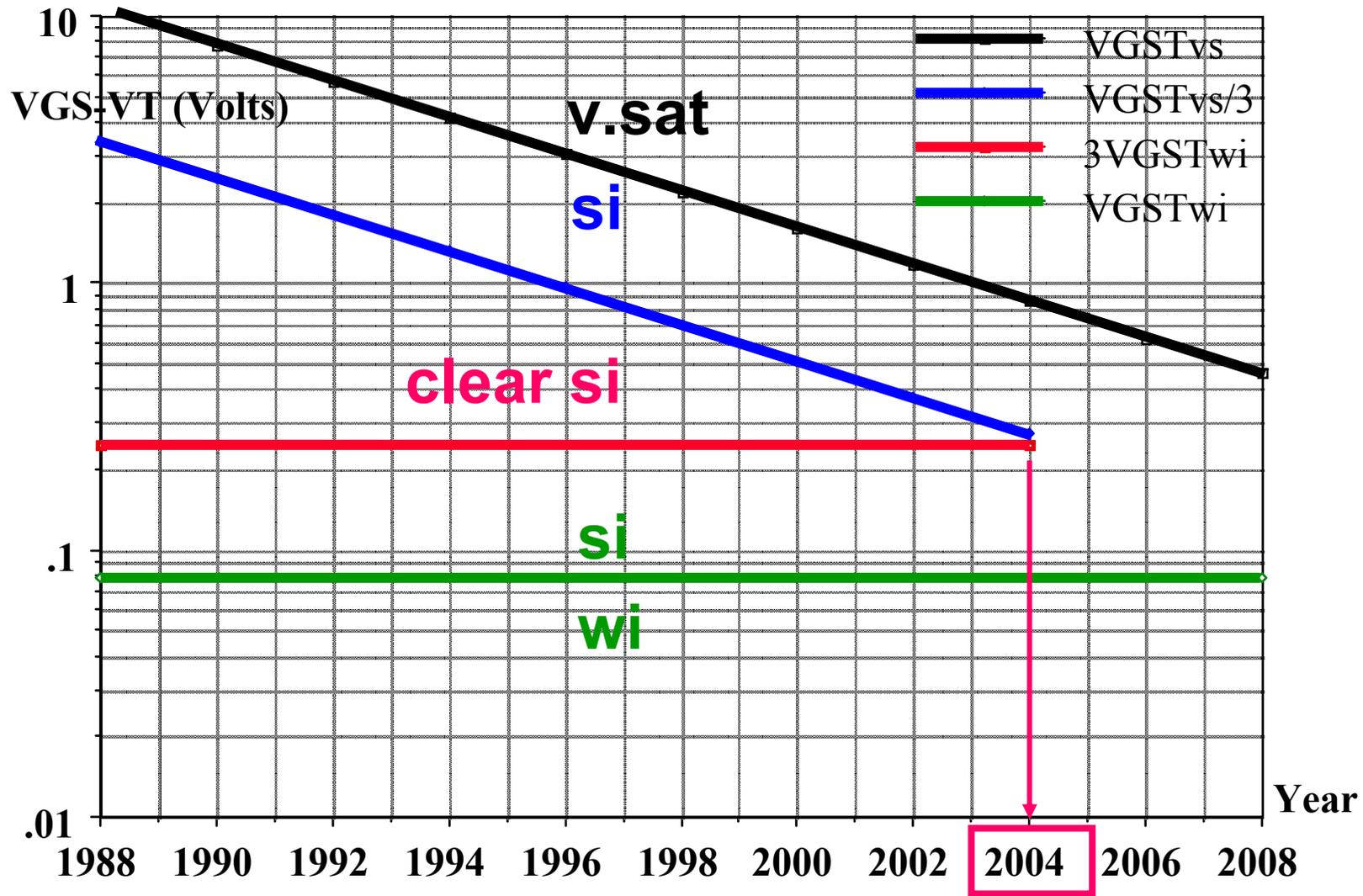
$$\frac{g_m}{W} \approx \frac{0.06 V_{GST}}{L^2 \text{ in } \mu\text{m}}$$

$$\frac{g_m}{W} = C_{ox} v_{sat}$$

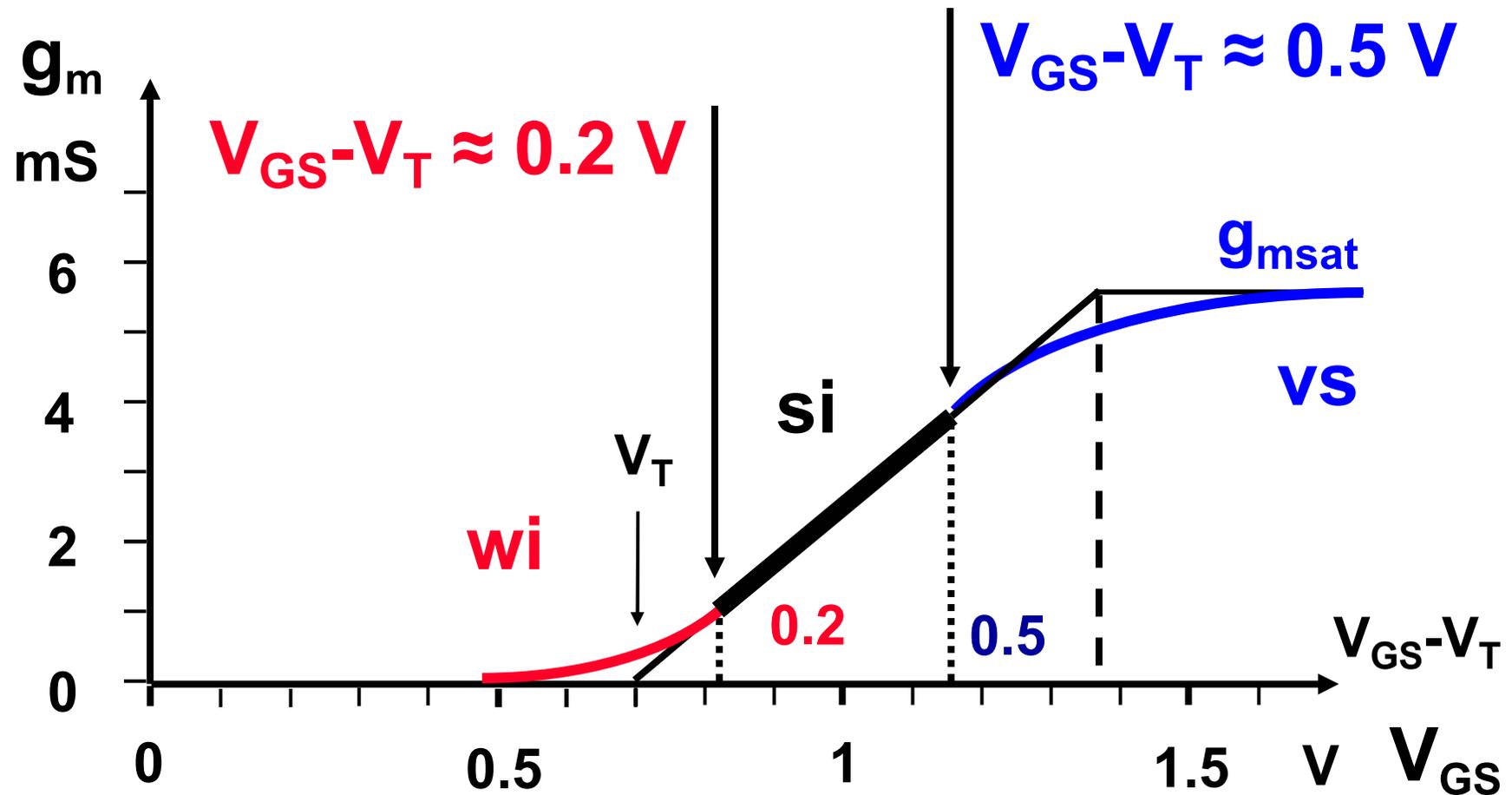
$$\frac{g_m}{W} \approx \frac{0.17}{L}$$

in μ m

Range of $V_{GS}-V_T$ values for si vs time

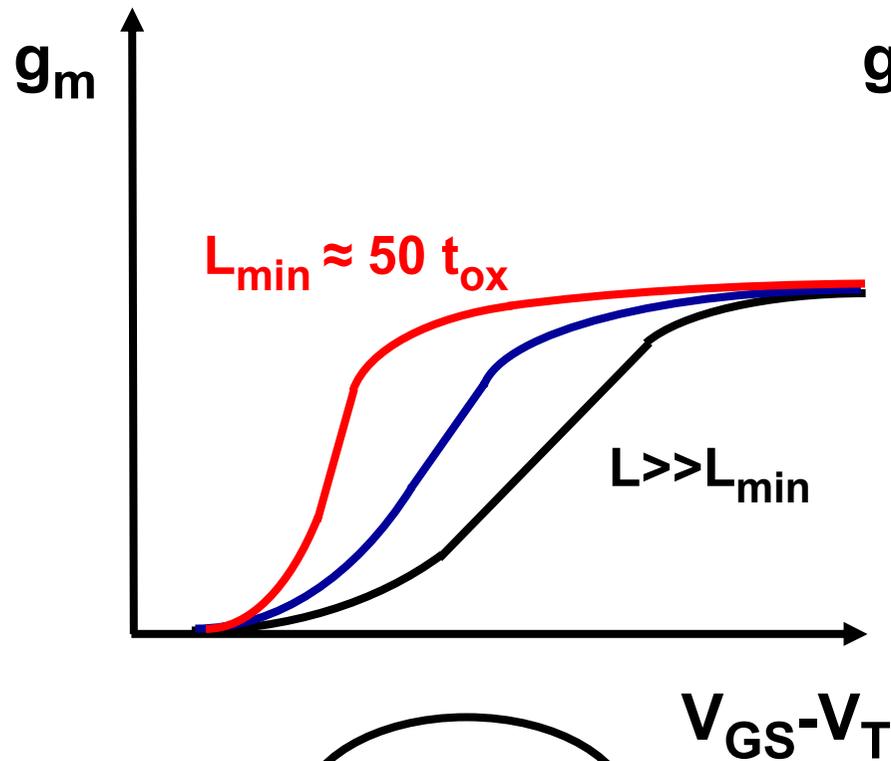


MOST operating region in si

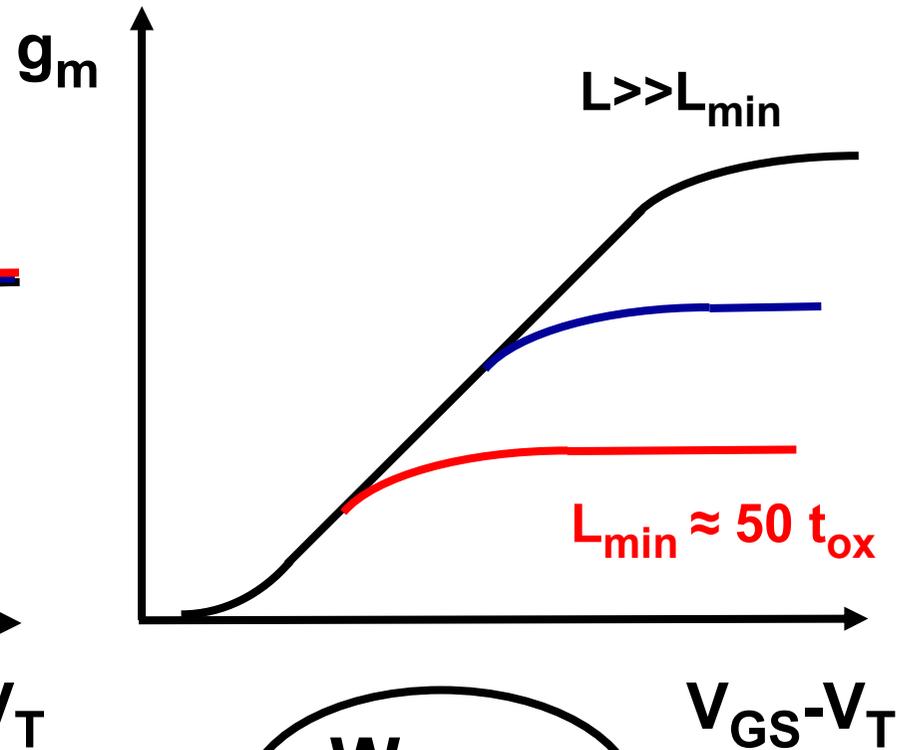


g_m vs V_{GS} for different L (same t_{ox})

Exercise :



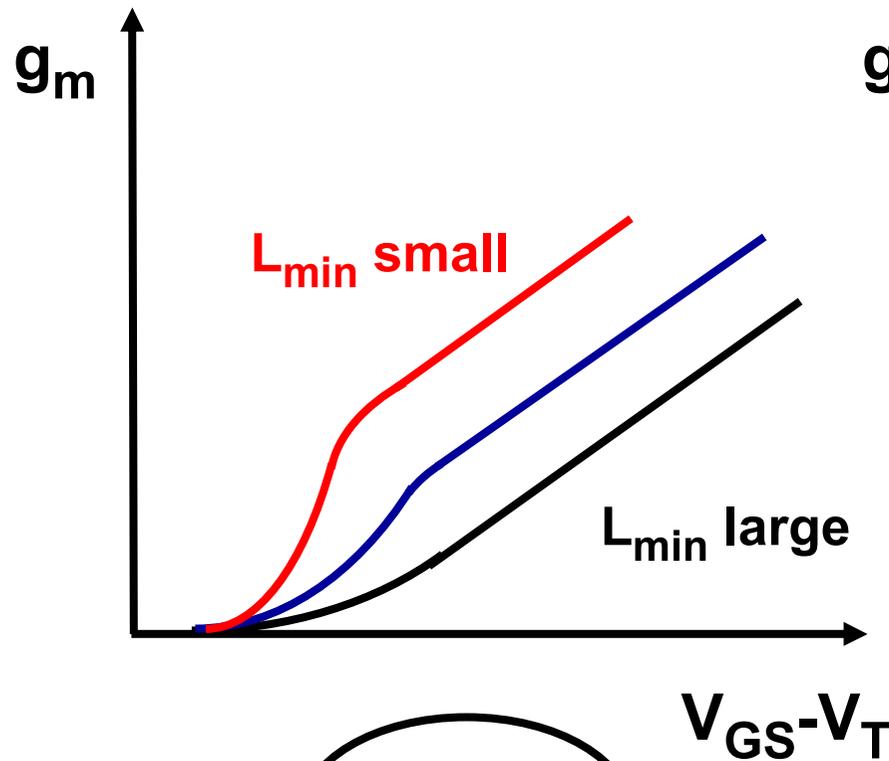
$$W = ct$$



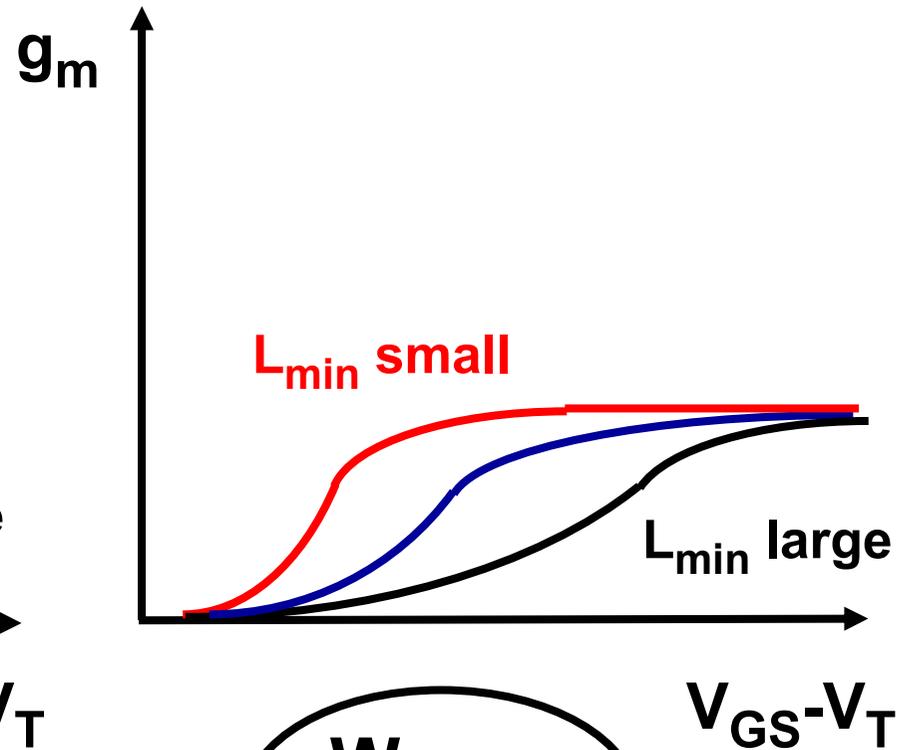
$$\frac{W}{L} = ct$$

g_m vs V_{GS} for different t_{ox} ($\approx L_{min}/50$)

Exercise :



$$W = ct$$



$$\frac{W}{L} = ct$$

Table : MOST I_{DS} , g_m & g_m/I_{DS}

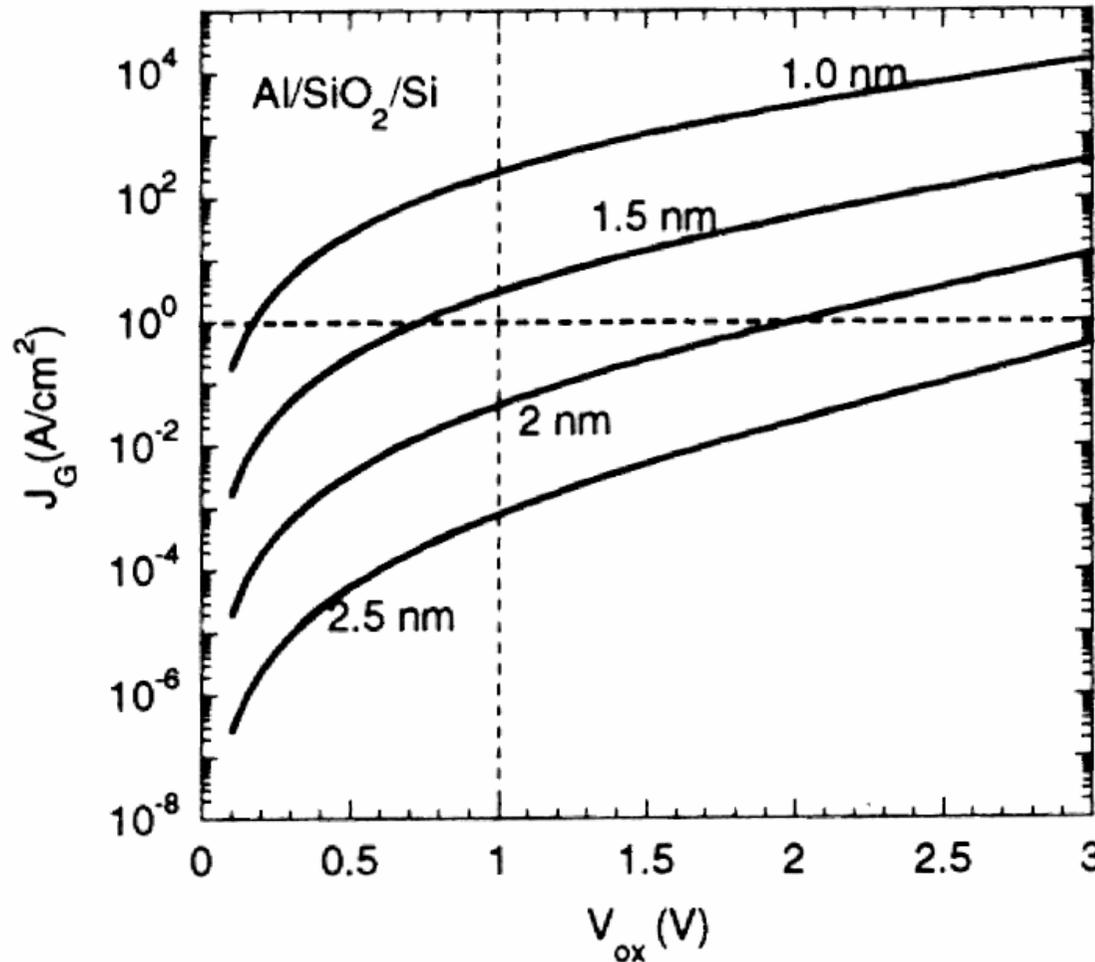
Summary :

TABLE 1-4 EXPRESSIONS OF I_{DS} , g_m AND g_m/I_{DS} FOR MOST

	I_{DS}	g_m	$\frac{g_m}{I_{DS}} = f(v_{GS} - V_T)$	$\frac{g_m}{I_{DS}} = f(I_{DS})$
wi	$I_{D0} \frac{W}{L} \exp\left(\frac{v_{GS}}{nkT/q}\right)$ (1-25a)	$\frac{I_{D0}}{nkT/q} \frac{W}{L} \exp\left(\frac{v_{GS}}{nkT/q}\right)$ (1-25b)	$\frac{1}{nkT/q}$ (1-26b)	$\frac{1}{nkT/q}$ (1-26b)
ws			$(v_{GS} - V_T)_{ws} = 2n \frac{kT}{q}$	$I_{DSws} = \frac{KP}{2n} \frac{W}{L} \left(2n \frac{kT}{q}\right)^2$
si	$\frac{KP}{2n} \frac{W}{L} (v_{GS} - V_T)^2$ (1-18c)	$2 \frac{KP}{2n} \frac{W}{L} (v_{GS} - V_T)$ (1-22a)	$\frac{2}{v_{GS} - V_T}$ (1-26a)	$2 \sqrt{\frac{KP}{2n} \frac{W}{L} \frac{1}{I_{DS}}}$ (1-26a)
sv			$(v_{GS} - V_T)_{sv} = \frac{2nLC_{ox}v_{sat}}{KP}$	$I_{DSsv} = \frac{2WLC_{ox}^2 v_{sat}^2}{KP/2n}$
vs	$WC_{ox} v_{sat} (v_{GS} - V_T)$ (1-38b)	$WC_{ox} v_{sat}$ (1-39)	$\frac{1}{v_{GS} - V_T}$	$\frac{WC_{ox} v_{sat}}{I_{DS}}$

Ref.: Laker, Sansen : Design of analog ..., MacGrawHill 1994; Table 1-4

Gate current



For 0.1 μm CMOS :

$t_{ox} \approx 2$ nm

$J_G \approx 4 \cdot 10^{-2}$ A/cm²

For 10 x 0.5 μm

$I_G \approx 2$ nA

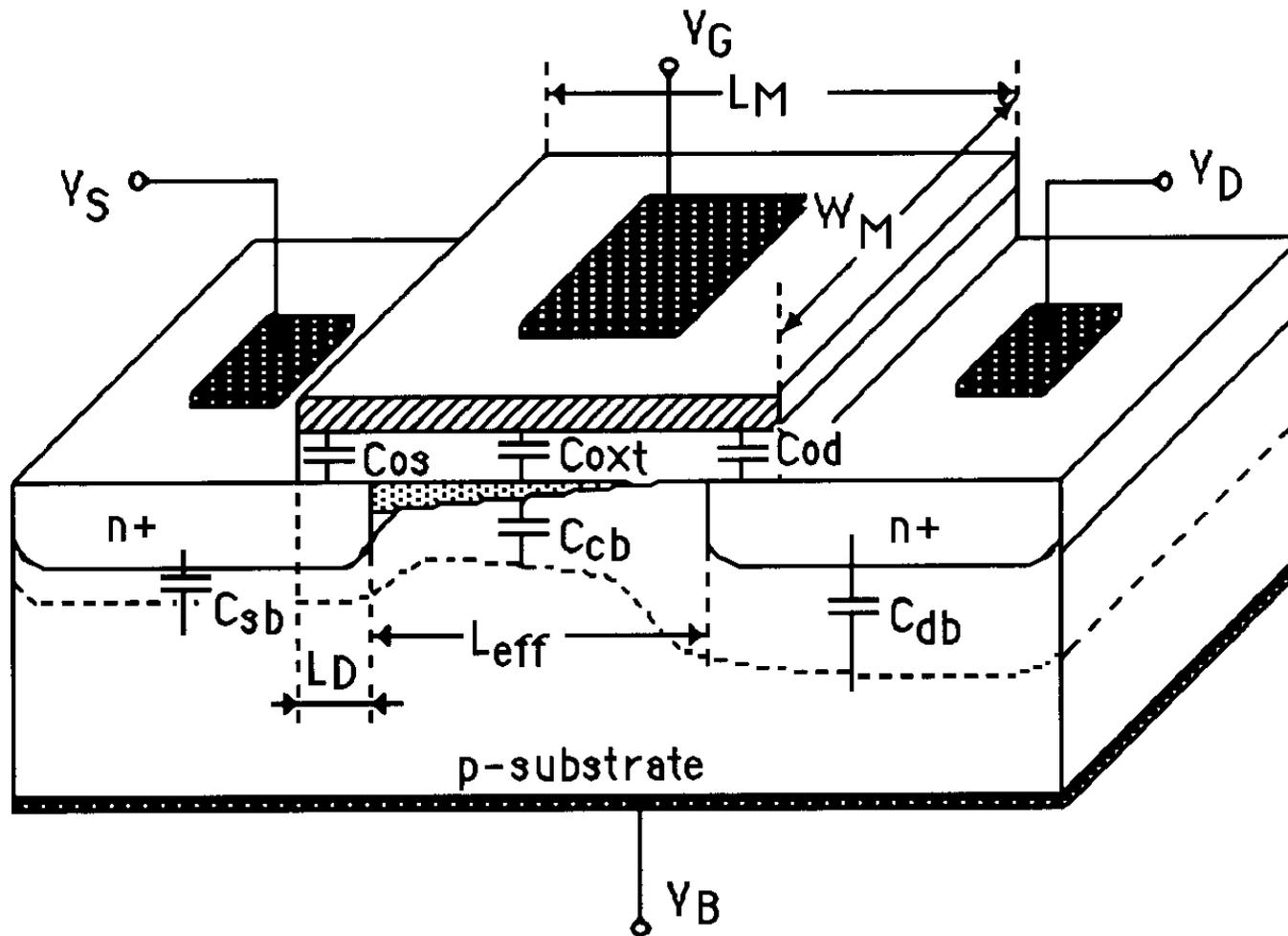
J_G (A/cm²)
 $\approx 4.5 \cdot 10^5 \exp\left(-\frac{L}{6.5}\right)$
L in nm

Ref. Koh, Tr ED 2001, 259-
Annema, JSSC Jan.05, 135.

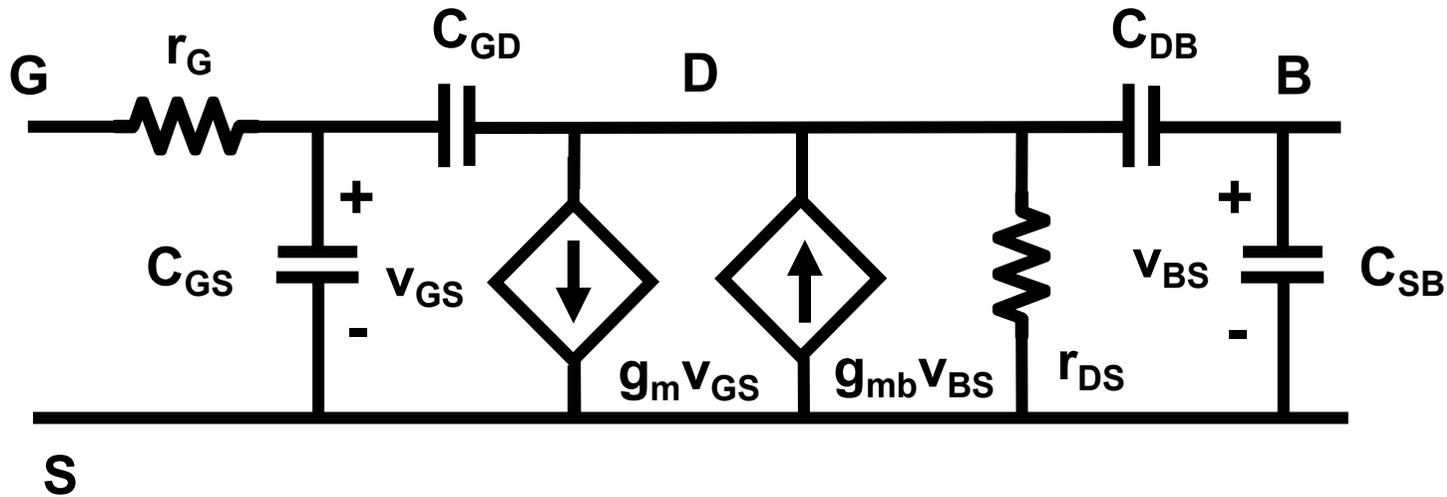
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- **Models of MOST transistors**
 - MOST as a resistor
 - MOST as an amplifier in strong inversion
 - Transition weak inversion-strong inversion
 - Transition strong inversion-velocity saturation
 - Capacitances and f_T
- **Models of Bipolar transistors**
- **Comparison of MOSTs & Bipolar transistors**

MOST capacitances



MOST capacitances C_{GS} & C_{GD}

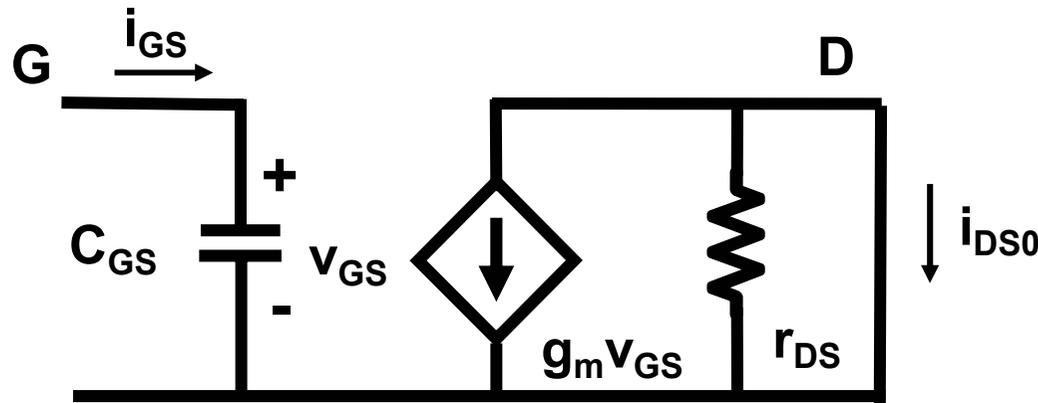


$$C_{GS} \approx \frac{2}{3} WLC_{ox} \approx 2W \text{ fF}/\mu\text{m for } L_{\min}$$

$$L_{\min} C_{ox} \approx L_{\min} \frac{\epsilon_{ox}}{t_{ox}} \approx 50 \epsilon_{ox} \approx 2 \text{ fF}/\mu\text{m}$$

$$C_{GD} = WC_{gdo}$$

MOST f_T where $i_{DS} = i_{GS}$



$$i_{GS} = v_{GS} C_{GS} s$$

$$i_{DS} = g_m v_{GS}$$

S

$$C_{GS} = \frac{2}{3} W L C_{ox} \quad g_m = 2K' \frac{W}{L} (V_{GS} - V_T) \quad K' = \frac{\mu C_{ox}}{2n}$$

$$f_T = \frac{g_m}{2\pi C_{GS}} = \frac{1}{2\pi} \frac{3}{2n} \frac{\mu}{L^2} (V_{GS} - V_T)$$

or $\approx \frac{v_{sat}}{2\pi L}$

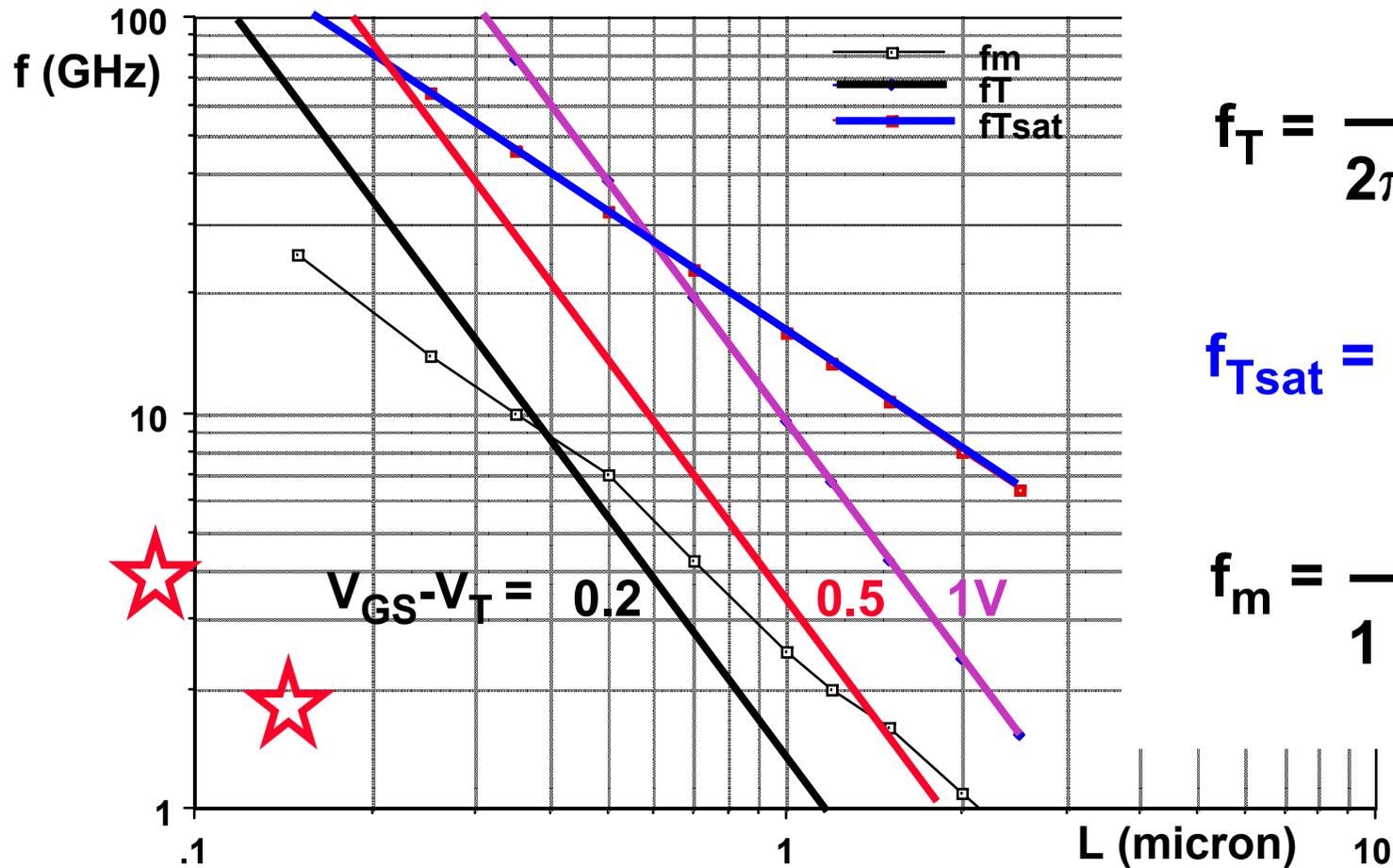
$$f_{max} \approx \sqrt{f_T / 8\pi r_G C_{GD}}$$

Design for high speed :

	High gain	High speed
$V_{GS}-V_T$	Low (0.2 V)	High (0.5 V)
L	High	Low

$V_{GS}-V_T$ sets the ratio g_m/I_{DS} !

Maximum f_T values versus channel length L



$$f_T = \frac{\mu}{2\pi L^2} \underbrace{(V_{GS} - V_T)}_{0.2 \dots 1 \text{ V}}$$

$$f_{Tsat} = \frac{V_{sat}}{2\pi L}$$

$$f_m = \frac{f_T}{1 + \alpha_{BD}}$$

$$\alpha_{BD} \approx \frac{C_{BD}}{C_{ox}}$$

Processors

f_T model in si and velocity saturation

$$f_T = \frac{g_m}{2\pi C_{GS}} \quad C_{GS} = kW \quad k = 2 \text{ fF}/\mu\text{m} = 2 \cdot 10^{-11} \text{ F/cm}$$
$$g_m = \frac{W}{L} \frac{17 \cdot 10^{-5}}{1 + 2.8 \cdot 10^4 L / V_{GST}} \quad L \text{ in cm}$$

$$f_T = \frac{1}{L} \frac{13.5}{1 + 2.8 L / V_{GST}} \text{ GHz}$$

L in μm

If $V_{GST} = 0.2 \text{ V}$, v_{sat} takes over for $L < 65 \text{ nm}$

If $V_{GST} = 0.5 \text{ V}$ for $L < 0.15 \mu\text{m}$

f_T model in si and weak inversion

$$f_T = \frac{g_m}{2\pi C_{GS}}$$

$$GM = \frac{g_m}{I_{DS}} \frac{nkT}{q} = \frac{1 - e^{-\sqrt{i}}}{\sqrt{i}}$$

$$g_m = \frac{I_{DS}}{nkT/q} \frac{1 - e^{-\sqrt{i}}}{\sqrt{i}} \quad \text{but } I_{DS} = i I_{DSt}$$

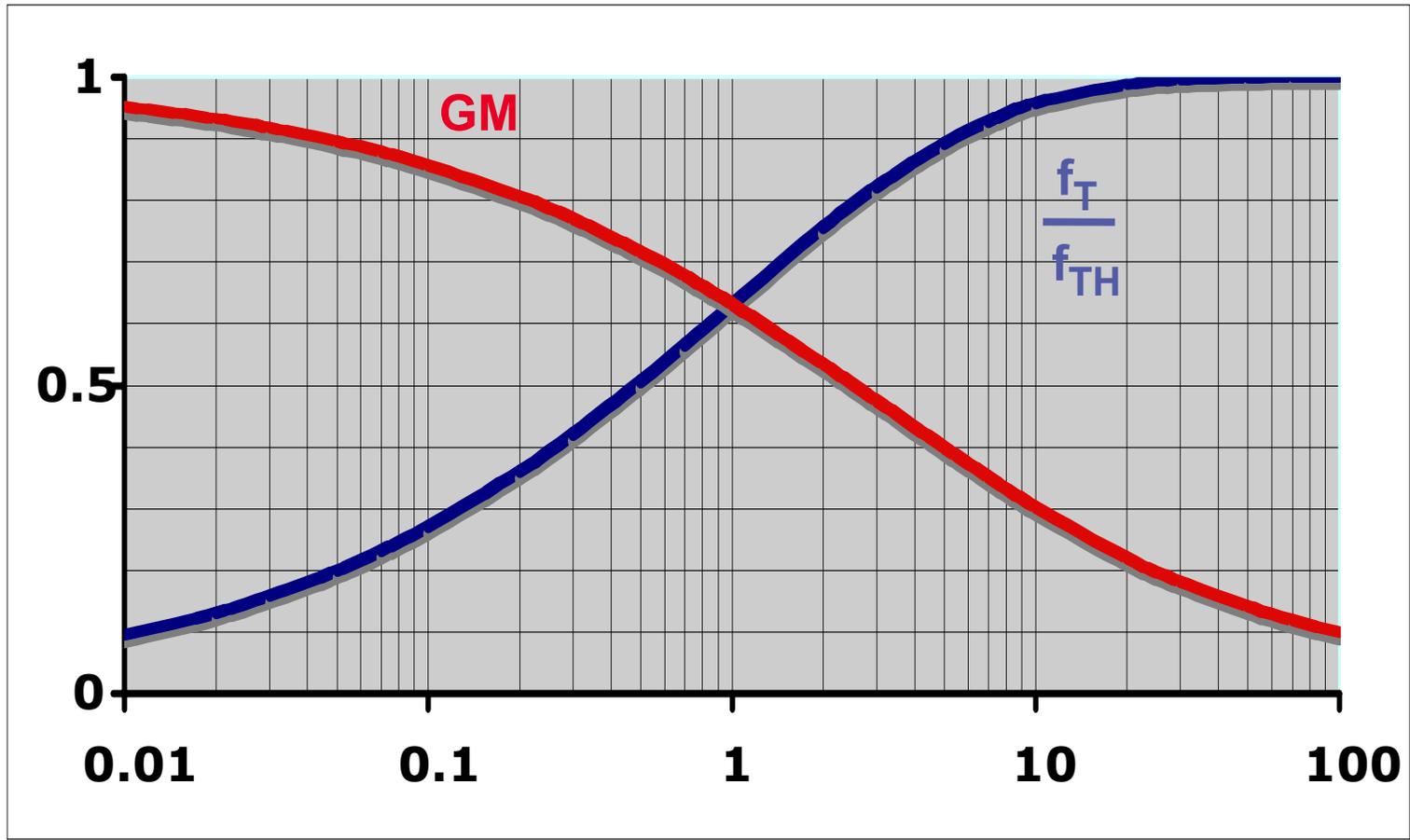
$$g_m = \frac{I_{DSt}}{nkT/q} \sqrt{i} (1 - e^{-\sqrt{i}})$$

$$\frac{f_T}{f_{TH}} = \sqrt{i} (1 - e^{-\sqrt{i}})$$

$\approx i$ for small i !

$$\begin{aligned} f_{TH} &= \frac{I_{DSt}}{2\pi C_{GS} nkT/q} = \frac{K' V_{GSTt}^2 W/L}{2\pi WL C_{ox} nkT/q} \\ &= \frac{4 K' nkT/q}{2\pi C_{ox} L^2} = \frac{2 \mu kT/q}{2\pi L^2} \end{aligned}$$

f_T versus inversion coefficient i



$$\frac{f_T}{f_{TH}} = \sqrt{i} (1 - e^{-\sqrt{i}})$$

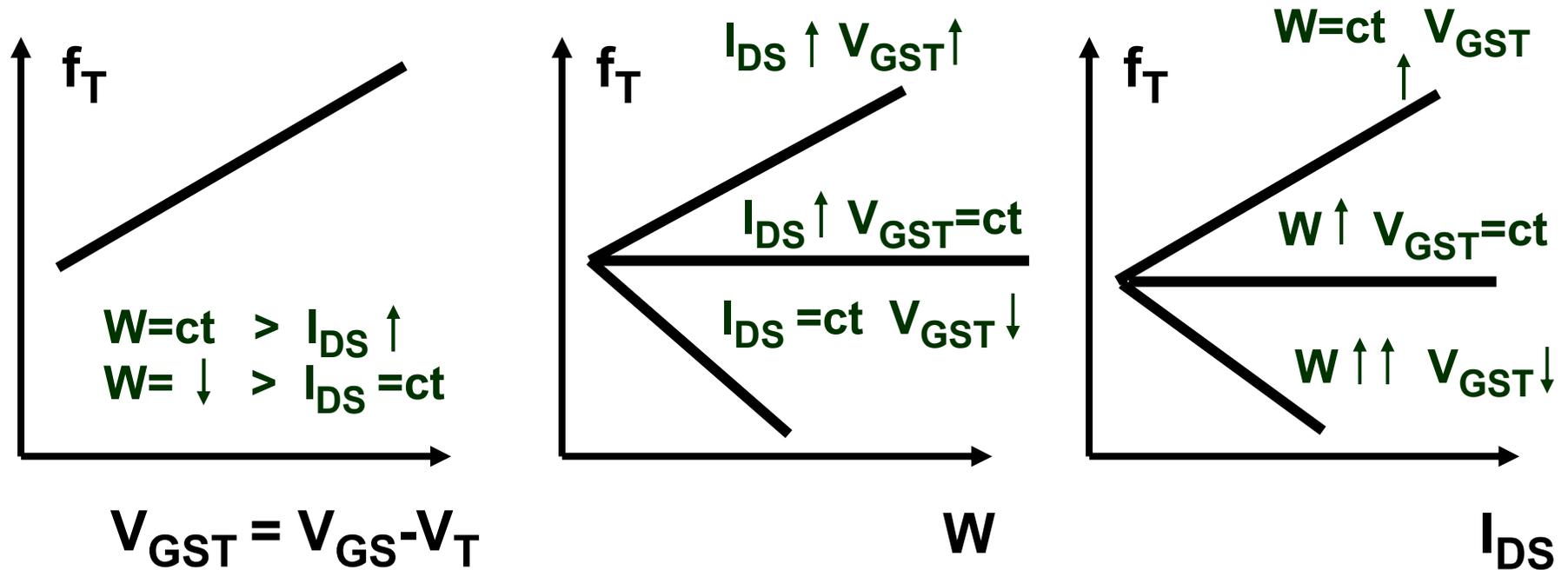
$$GM = \frac{1 - e^{-\sqrt{i}}}{\sqrt{i}}$$

$$i = \frac{I_{DS}}{I_{DSt}}$$

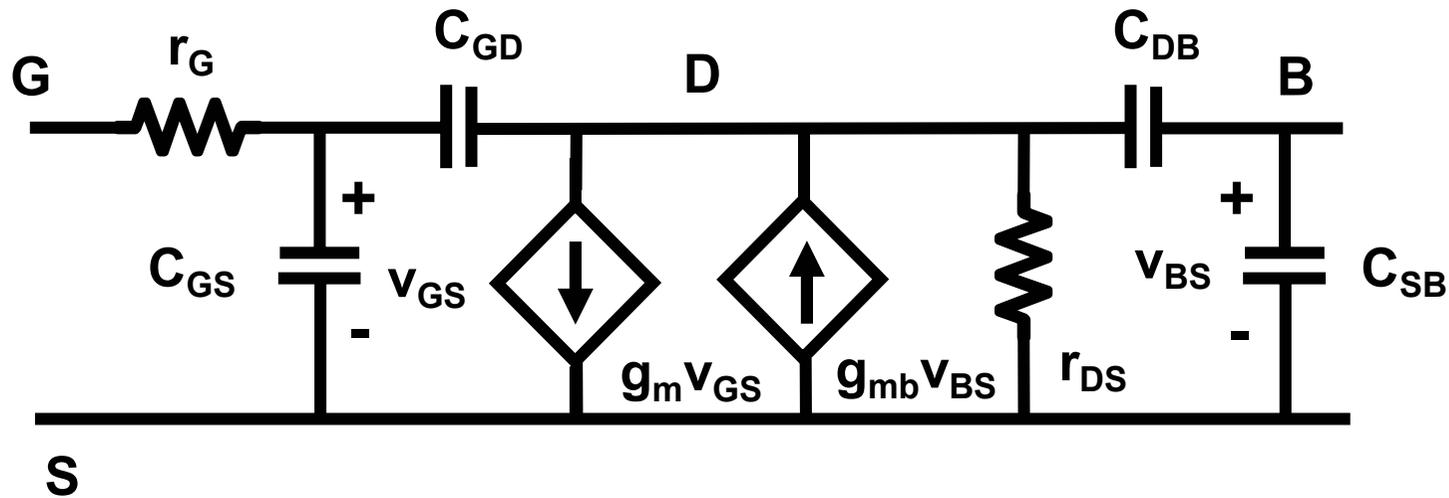
Exercise: MOST f_T or not f_T ?

all $L = L_{\min}$

$$f_T = \frac{1}{2\pi} \frac{\mu}{L^2} (V_{GS} - V_T) = \frac{\sqrt{K' I_{DS}}}{\pi C_{ox} \sqrt{WL^3}} = \frac{I_{DS}}{\pi W L C_{ox} (V_{GS} - V_T)}$$



MOST capacitances C_{SB} & C_{DB}

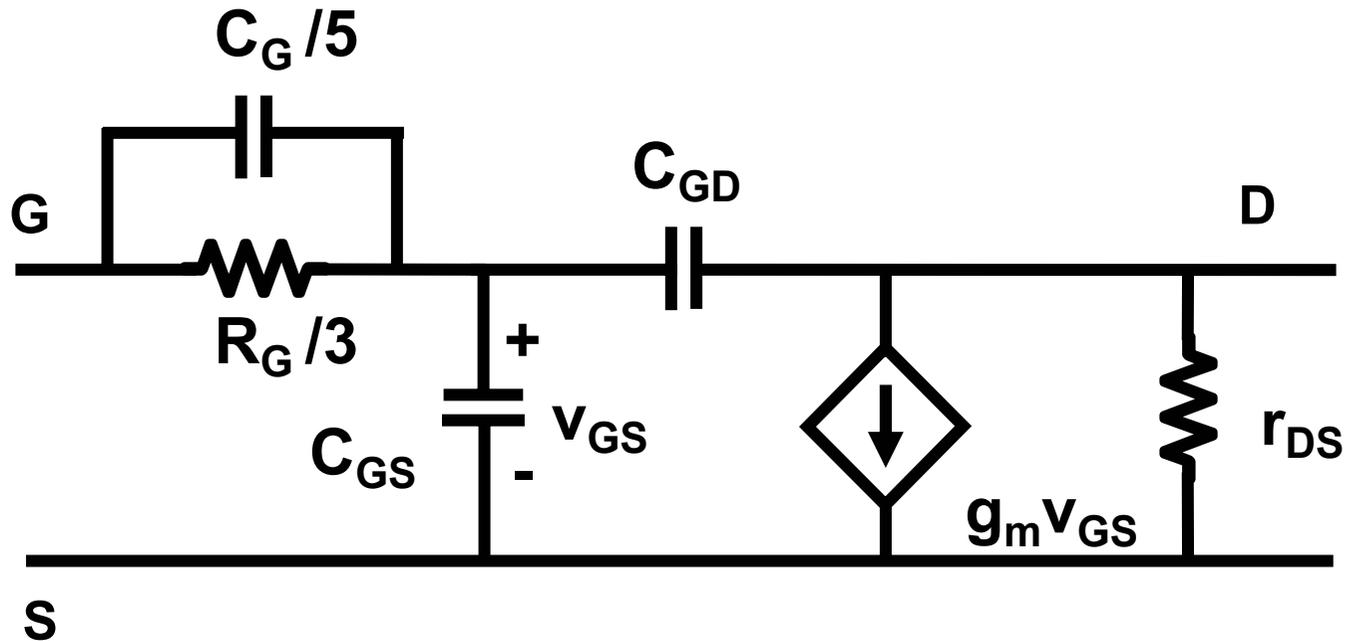


$$C_{SB} = \frac{C_{jSB0}}{\sqrt{1 + V_{SB}/\phi_{jS}}}$$

$$\phi_{jS} \approx \phi_{jD} \approx 0.5 \dots 0.7 \text{ V}$$

$$C_{DB} = \frac{C_{jDB0}}{\sqrt{1 + V_{DB}/\phi_{jD}}}$$

RF MOST model



$$C_G = C_{GS} + C_{GD}$$

Ref. Tin, Tr. CAD, April 1998, 372

Ref. Sansen, etal, ACD, XDSL,
RFMOS models, Kluwer 1999

Single-page MOST model

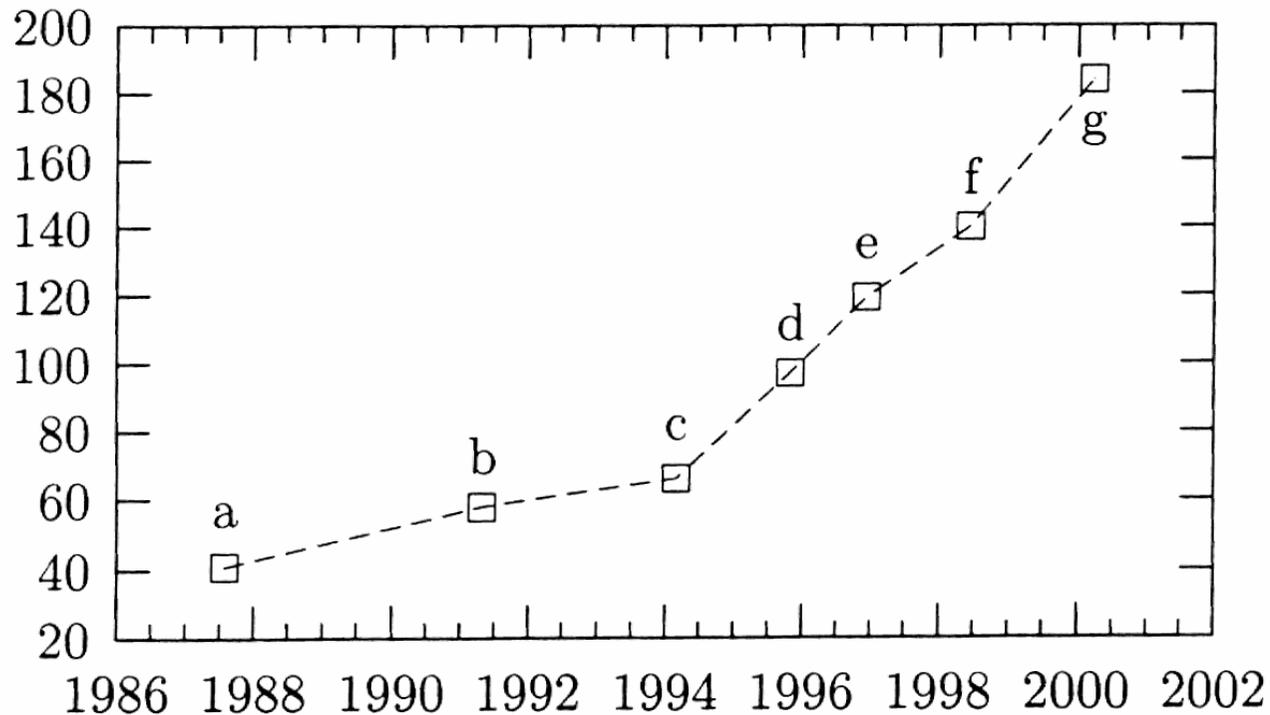
$$I_{DS} = K'_n \frac{W}{L} (V_{GS} - V_T)^2 \quad V_{GS} - V_T \approx 0.2 \text{ V} \quad \begin{array}{l} K'_n \approx 100 \mu\text{A}/\text{V}^2 \\ K'_p \approx 40 \mu\text{A}/\text{V}^2 \end{array}$$

$$g_m = 2K'_n \frac{W}{L} (V_{GS} - V_T) = 2 \sqrt{K'_n \frac{W}{L} I_{DS}} = \frac{2 I_{DS}}{V_{GS} - V_T}$$

$$r_{DS} = r_o = \frac{V_{EL}}{I_{DS}} \quad \begin{array}{l} V_{En} \approx 5 \text{ V}/\mu\text{mL} \quad V_{Ep} \approx 8 \text{ V}/\mu\text{mL} \\ v_{\text{sat}} = 10^7 \text{ cm/s} \end{array}$$

$$f_T = \frac{1}{2\pi} \frac{3}{2n} \frac{\mu}{L^2} (V_{GS} - V_T) \quad \text{or now} \approx \frac{v_{\text{sat}}}{2\pi L}$$

Growing number of parameters !



a: BSIM1
b: BSIM2
c: BSIM3 version 2.0
d: BSIM3 version 3.0
e: BSIM3 version 3.1
f: BSIM3 version 3.2.2
g: BSIM4.0.0

BSIM4 : http://www-device.eecs.berkeley.edu/bsim/bsim_ent.html

Model 11 : http://www.semiconductors.philips.com/Philips_Models/mos_models

EKV : <http://legwww.epfl.ch/ekv/model.html> </model11/index.html>

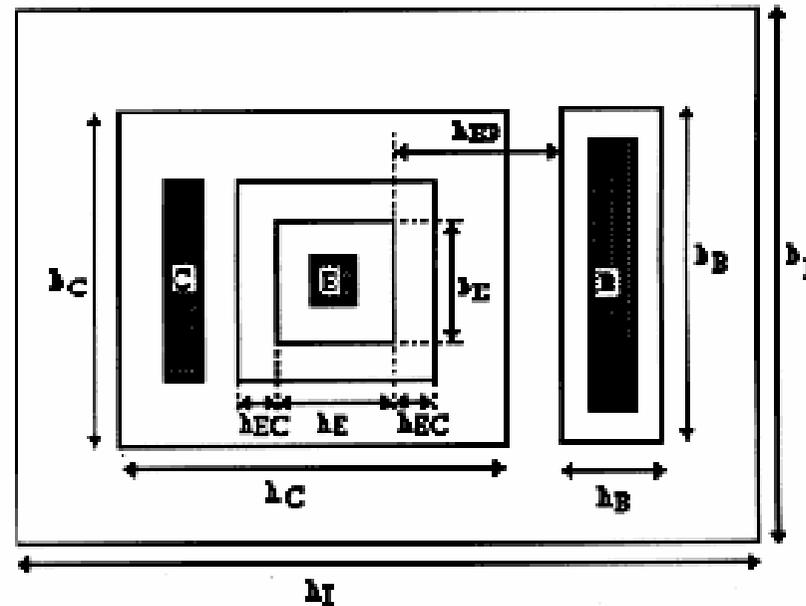
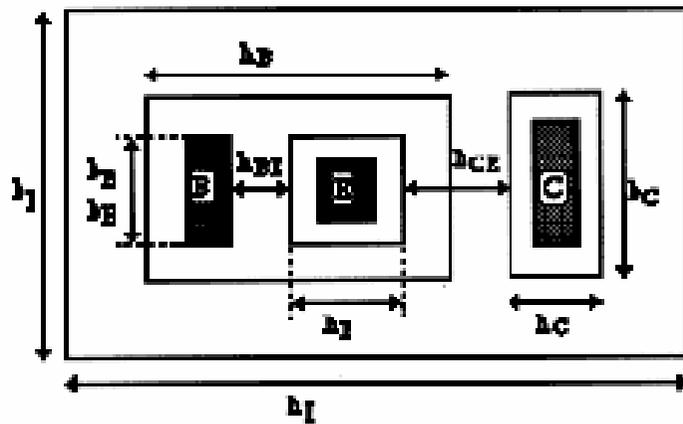
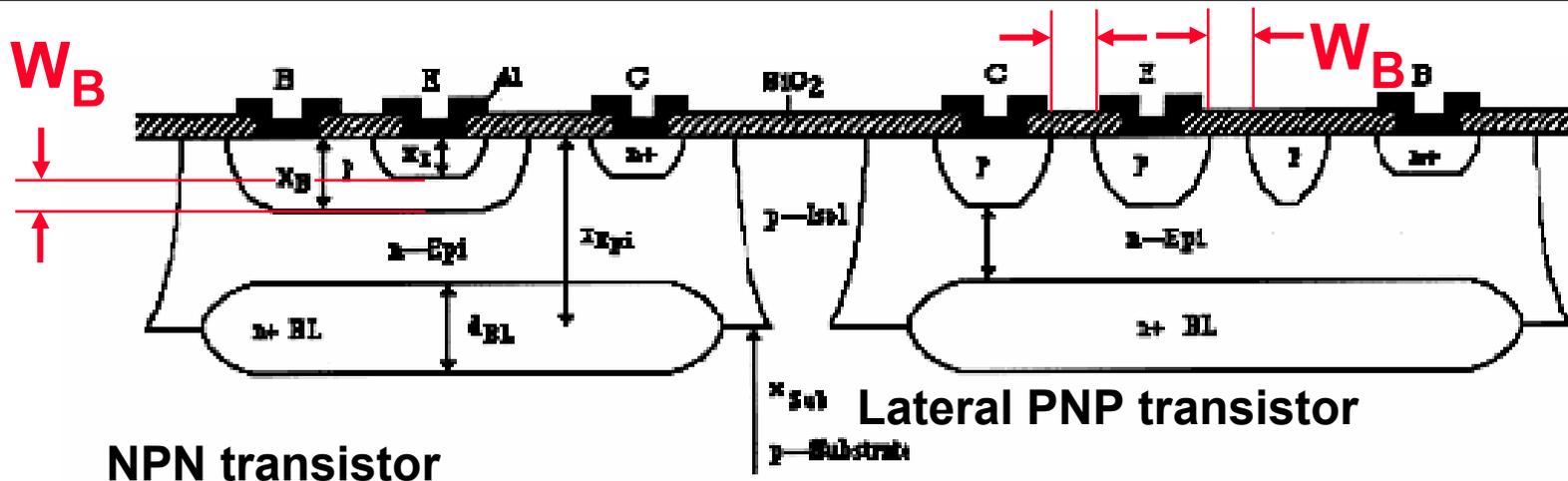
Benchmark tests

1. Weak inversion transition for I_{DS} and g_m/I_{DS} ratio
2. Velocity saturation transition for I_{DS} and g_m/I_{DS} ratio
3. Output conductance around V_{DSsat}
4. Continuity of currents and caps around zero V_{DS}
5. Thermal and 1/f noise
6. High frequency input impedance (s_{11}) and transimpedance (s_{21})

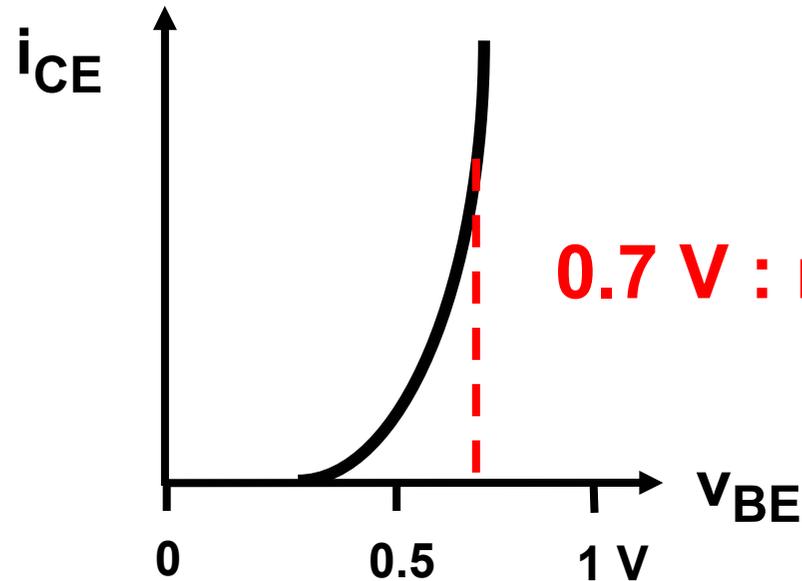
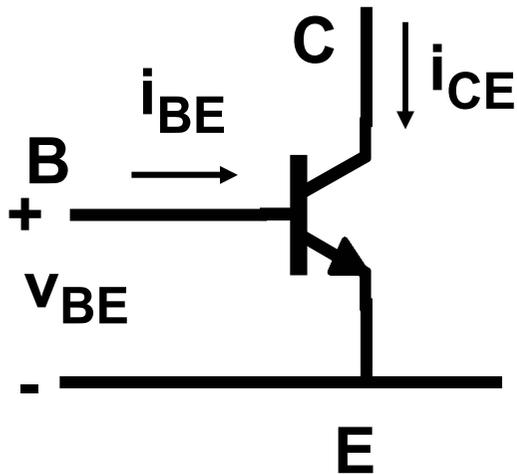
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- **Models of MOST transistors**
- **Models of Bipolar transistors**
- **Comparison of MOSTs & Bipolar transistors**

□ Bipolar transistors



Bipolar transistor I_{CE} versus V_{BE}



$$I_{CE} = I_S \exp \frac{V_{BE}}{kT/q}$$

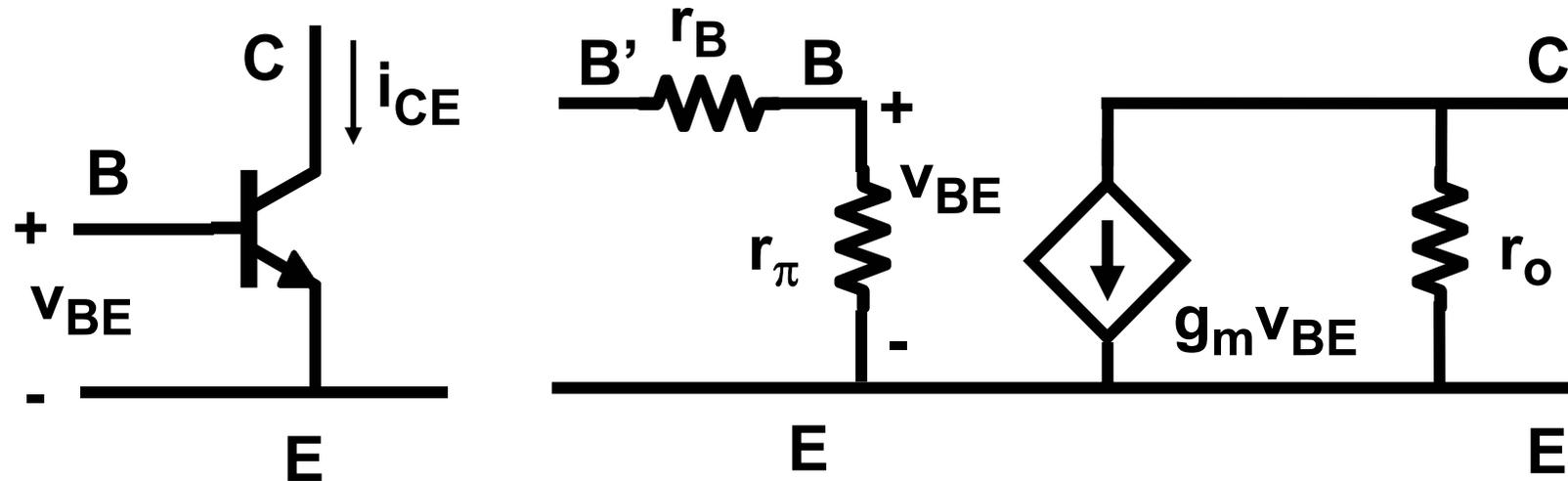
$$I_S \approx 10^{-15} \text{ A} \quad kT/q = 26 \text{ mV at } 300 \text{ K}$$

$$I_{BE} = \frac{I_{CE}}{\beta}$$

is leakage current

$$\beta \approx 10 \dots 1000$$

Bipolar transistor small-signal model : g_m & r_o



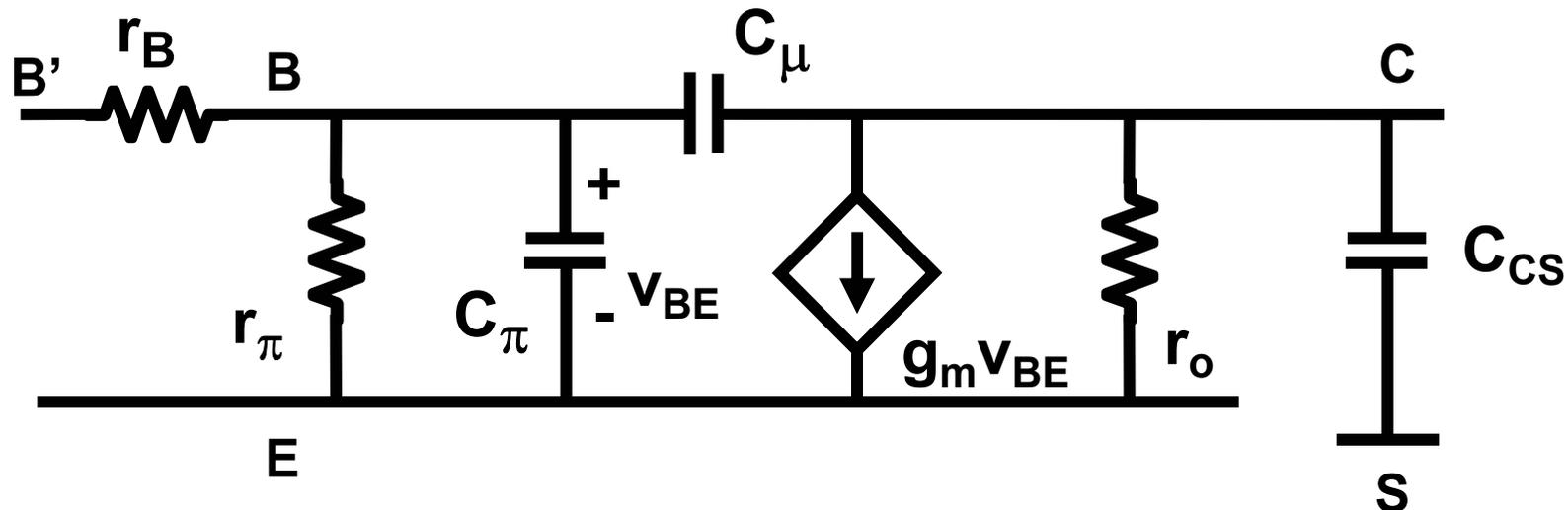
$$g_m = \frac{di_{CE}}{dv_{BE}} = \frac{I_{CE}}{kT/q}$$

$$\frac{g_m}{I_{CE}} = \frac{1}{kT/q} \approx 40 \text{ V}^{-1}$$

$$r_\pi = \frac{dv_{BE}}{di_{BE}} = \beta \frac{dv_{BE}}{di_{CE}} = \frac{\beta}{g_m}$$

$$r_o = \frac{V_E}{I_{CE}} \quad \begin{array}{l} V_{En} \approx 20 \text{ V} \\ V_{Ep} \approx 10 \text{ V} \end{array}$$

Bipolar transistor capacitance C_π



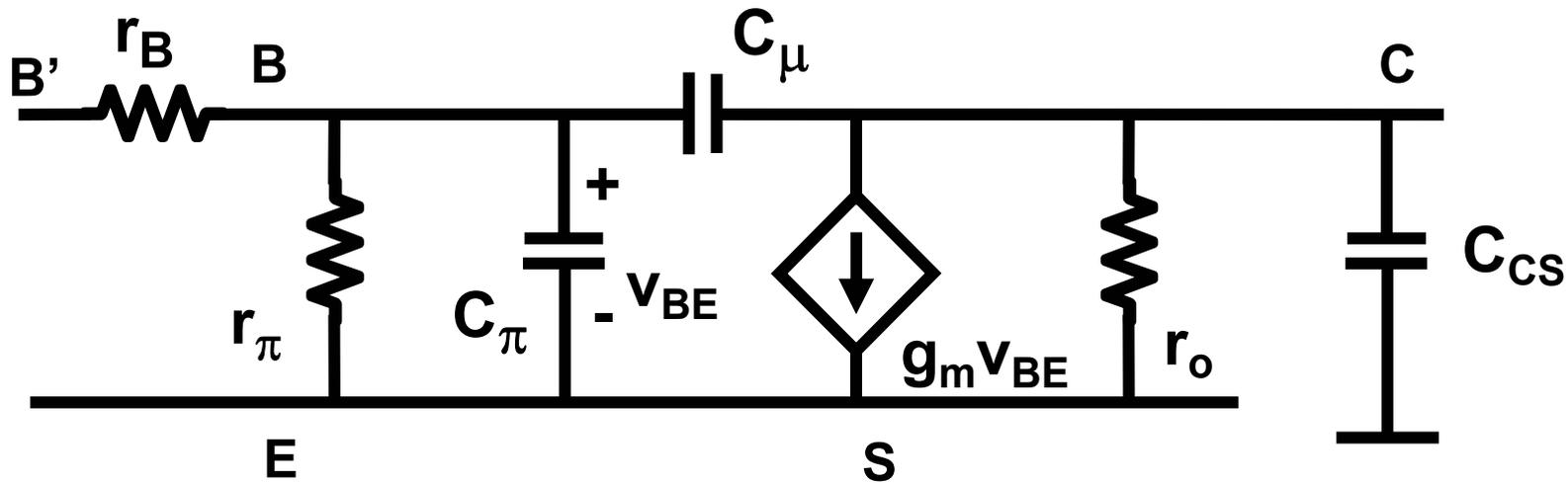
$$C_\pi = C_{jBE} + C_D$$

$$C_{jBE} = \frac{C_{jBE0}}{\sqrt{1 + V_{BE}/\phi_{jE}}}$$

$$\phi_{jE} \approx 0.7 \text{ V}$$

C_D is the diffusion capacitance

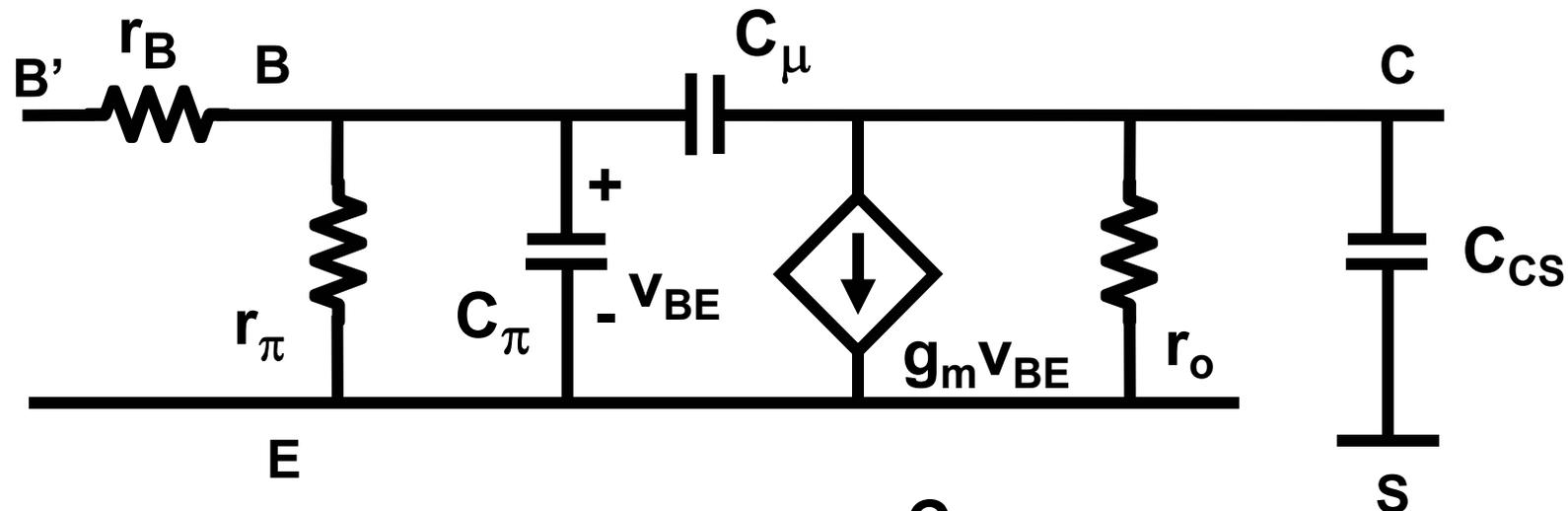
Diffusion capacitance C_D



$$C_D = \frac{Q_B}{V_{BE}} = \tau_F \frac{di_{CE}}{dv_{BE}} = \tau_F g_m = \tau_F \frac{I_{CE}}{kT/q}$$

Base transit time $\tau_F = \frac{W_B^2}{2D_n}$ or now $\approx \frac{W_B}{v_{sat}}$
 $\approx 10 \dots 200 \text{ ps}$

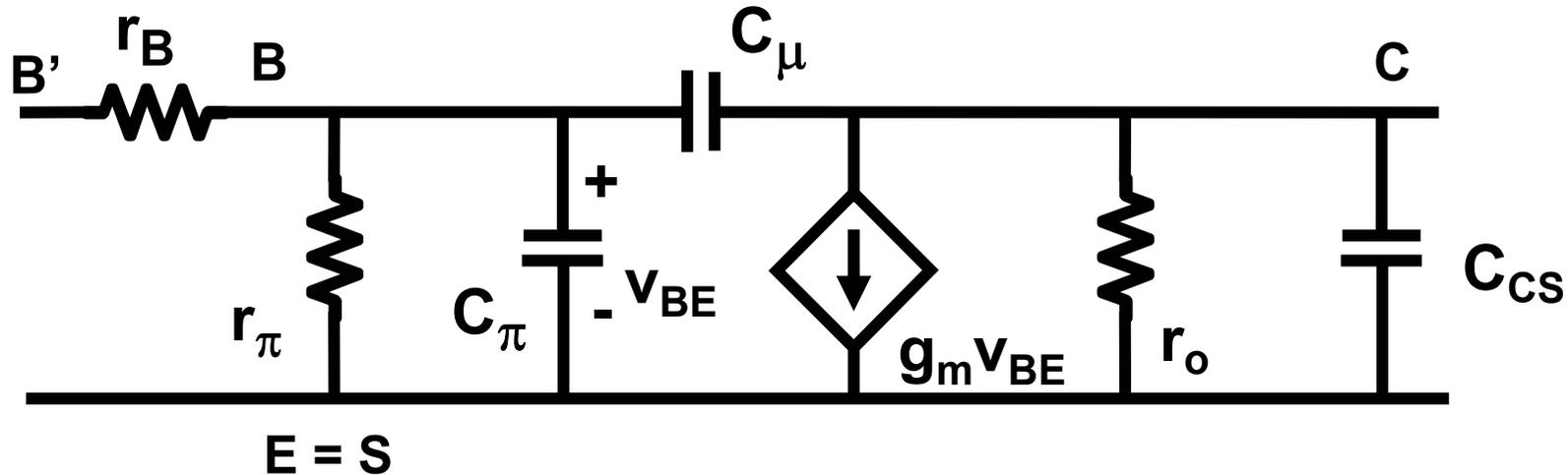
Bipolar transistor capacitances C_μ & C_{cs}



$$C_\mu = C_{jBC} \quad C_{jBC} = \frac{C_{jBC0}}{\sqrt{1 + V_{BC}/\phi_{jC}}}$$

$$C_{cs} = C_{jCS} \quad C_{jCS} = \frac{C_{jCS0}}{\sqrt{1 + V_{CS}/\phi_{jS}}} \quad \phi_{jC} \approx \phi_{jS} \approx 0.5 \text{ V}$$

Bipolar transistor f_T

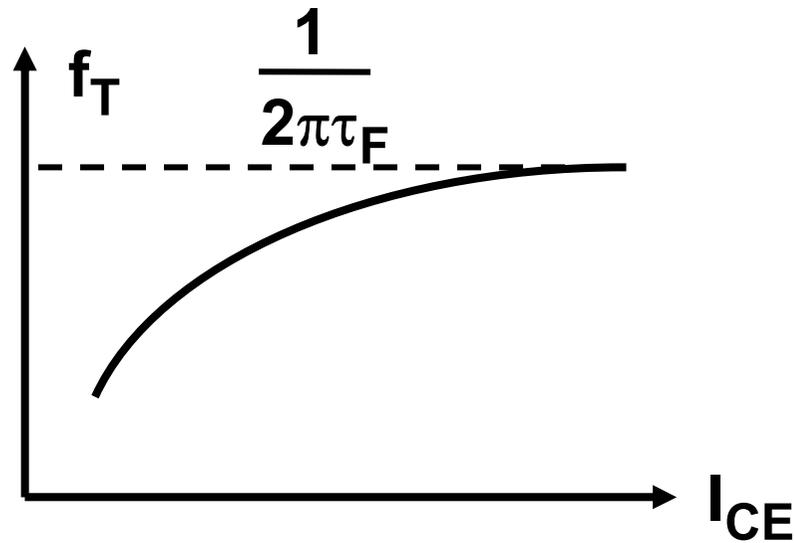


$$f_T = \frac{g_m}{2\pi C_\pi} = \frac{1}{2\pi} \frac{1}{\tau_F + \frac{C_{jBE} + C_\mu}{g_m}} \quad \text{or } \approx \frac{V_{sat}}{2\pi W_B}$$

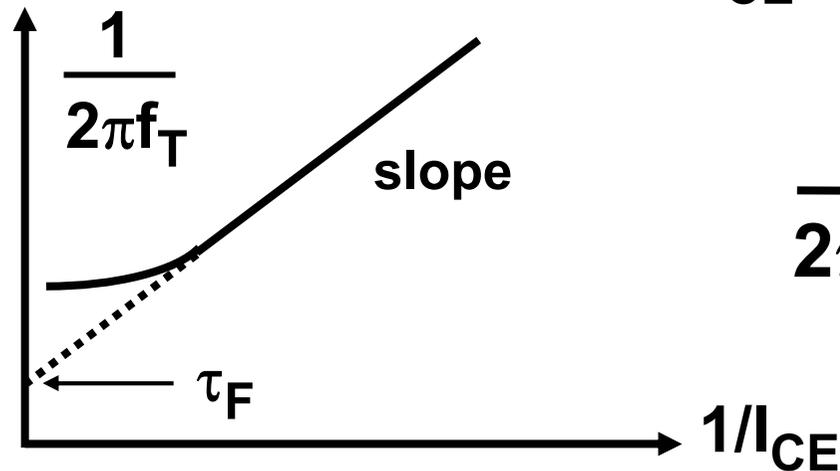
For a current drive !

$$f_{max} \approx \sqrt{f_T / 8\pi r_B C_\mu}$$

Bipolar transistor f_T versus I_{CE}



$$f_T = \frac{1}{2\pi} \frac{1}{\tau_F + \frac{C_{jBE} + C_\mu}{g_m}}$$



$$\frac{1}{2\pi f_T} = \tau_F + \underbrace{(C_{jBE} + C_\mu) \frac{kT}{q}}_{\text{slope}} \frac{1}{I_{CE}}$$

Single-page Bipolar transistor model

$$I_{CE} = I_S \exp \frac{V_{BE}}{kT/q} \quad I_S \approx 10^{-15} \text{ A} \quad kT/q = 26 \text{ mV at 300 K}$$

$$g_m = \frac{I_{CE}}{kT/q} \quad r_o = \frac{V_E}{I_{CE}} \quad V_{En} \approx 20 \text{ V} \quad V_{Ep} \approx 10 \text{ V}$$

$$f_T = \frac{1}{2\pi} \frac{1}{\tau_F + \frac{C_{je} + C_{jc}}{g_m}} \quad \text{or } \approx \frac{V_{sat}}{2\pi W_B}$$

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- **Models of MOST transistors**
- **Models of Bipolar transistors**
- **Comparison of MOSTs and Bipolars**

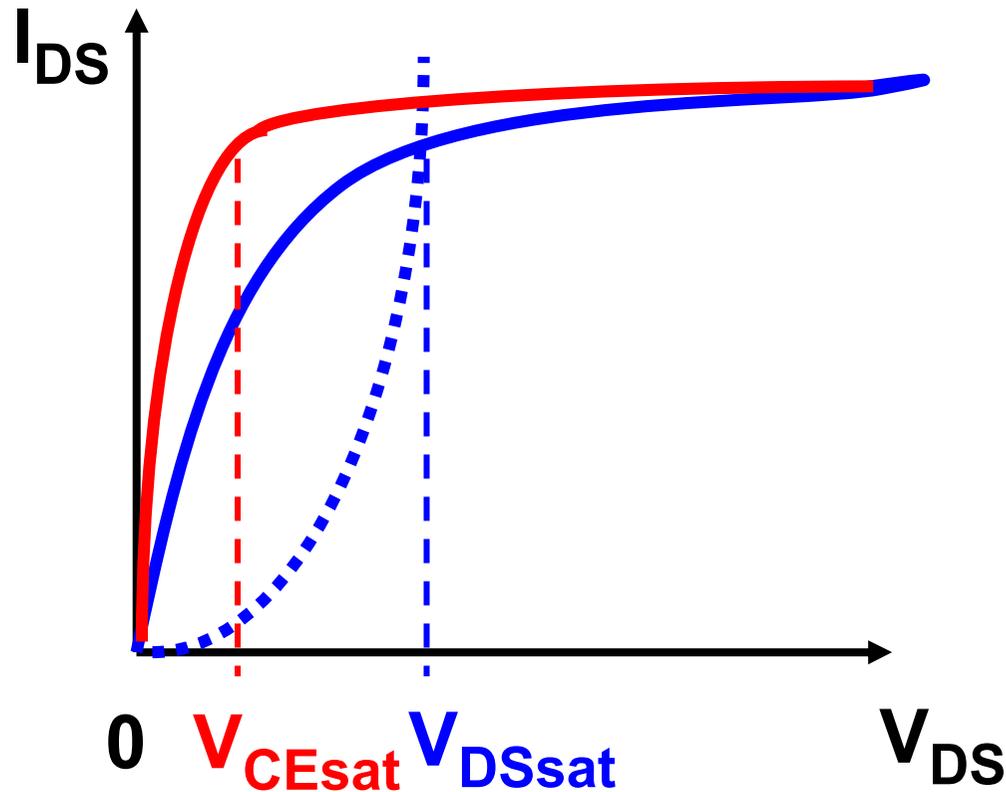
Comparison MOST - Bipolar

TABLE 2-8 COMPARISON OF MOSTS AND BIPOLAR TRANSISTORS

	Specification		MOST	Bipolar transistor	
1.	I_{IN} R_{IN}		0 ∞	I_C / β $r_{\pi} + r_B$	$\beta ?$
2.	V_{DSsat}		$V_{GS} - V_T = \sqrt{\frac{I_{DS}}{K'W/L}}$	few kT/q	
3.	$\frac{g_m}{I}$	wi	$\frac{1}{nkT/q}$	$\frac{1}{kT/q}$	$n = 1 + \frac{C_D}{C_{ox}}$
		si	$\frac{2}{V_{GS} - V_T}$	$\frac{1}{kT/q}$	4... 6 x
		vs	$\frac{1}{V_{GS} - V_T}$	$\frac{1}{kT/q}$	

Ref. Laker Sansen Table 2-8

Comparison MOST - Bipolar : minimum V_{DS}



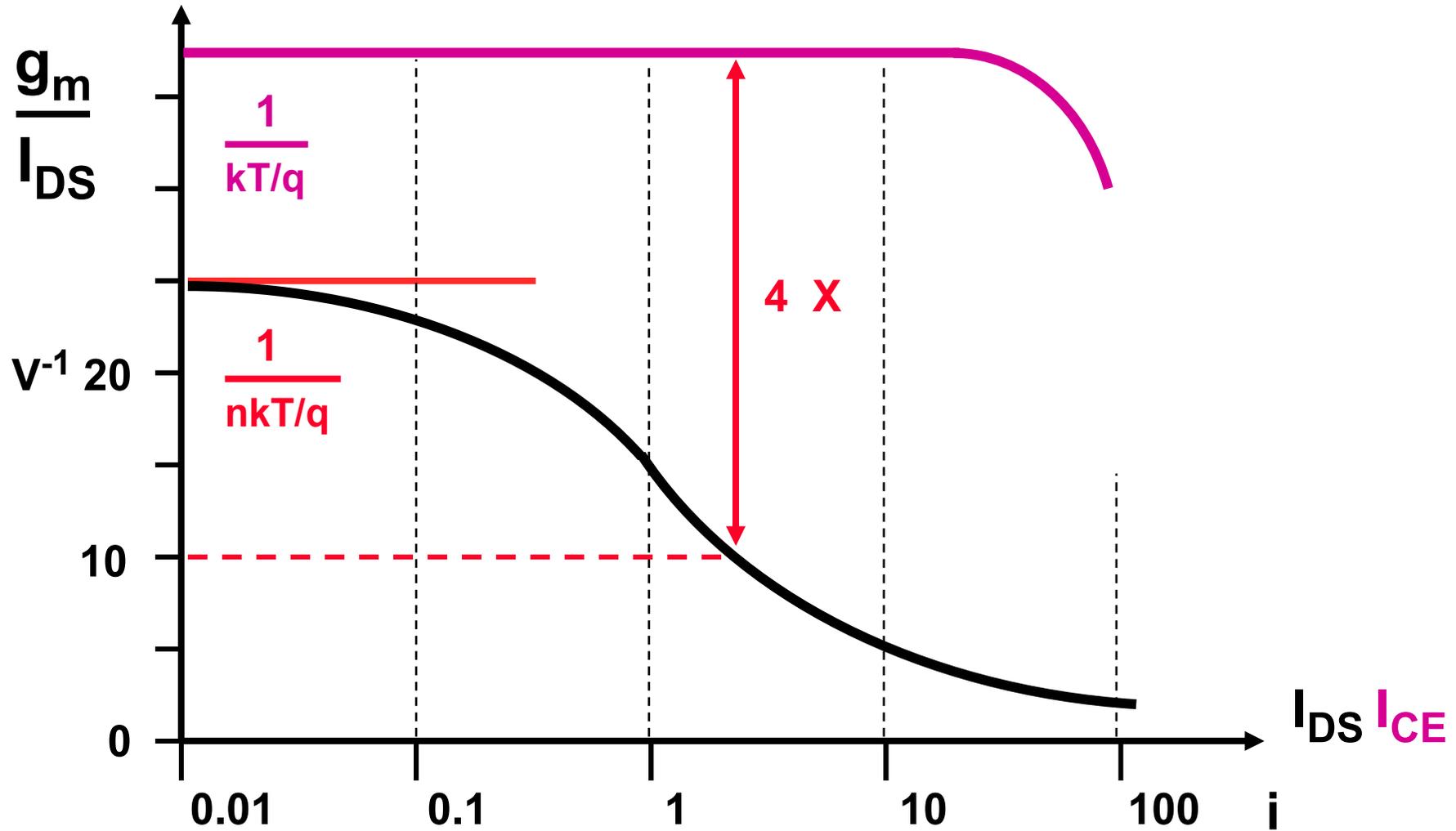
$$V_{DSsat} \approx V_{GS} - V_T$$

$$V_{GS} - V_T \approx \sqrt{\frac{I_{DS}}{K'_n \frac{W}{L}}}$$

$$V_{CEsat} \approx kT/q's$$

Ref. Laker - Sansen Table 2-8

Comparison MOST - Bipolar : g_m/I_{DS} ratio



Design plan for g_m :

$$I_{DS} = K'_n \frac{W}{L} (V_{GS} - V_T)^2$$

$$g_m = 2K'_n \frac{W}{L} (V_{GS} - V_T) = 2 \sqrt{K'_n \frac{W}{L} I_{DS}} = \frac{2 I_{DS}}{V_{GS} - V_T}$$

4 variables with 2 equations >> 2 free variables

Choose $V_{GS} - V_T$ and L !



Comparison MOST - Bipolar

4.	Design planning		$L, V_{GS} - V_T$	kT/q
5.	I -range		1 decade	7 decades
6.	Max f_T	low I high I	C_{GS}, C_{GD} v_{sat}/L_{eff}	C_{jEt}, C_{μ} v_{sat}/W_B
7.	Noise $\overline{dv_i^2}$	Therm.	$4kT \left(\frac{2/3}{g_m} + R_G \right)$	$4kT \left(\frac{1/2}{g_m} + R_B \right)$
	Offset	$1/f$	$10\times$ $10\times$	

$$v_{sat} \approx 10^7 \text{ cm/s}$$

Ref. Laker Sansen Table 2-8

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Reference books on Transistor models

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